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# PHYSICAL CHEMISTRY

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**Abstract**

**Full Text**

## PHYSICAL CHEMISTRY

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### ON THE UPPER LIMIT OF SELF-IGNITION IN A CHAIN UNBRANCHED REACTION

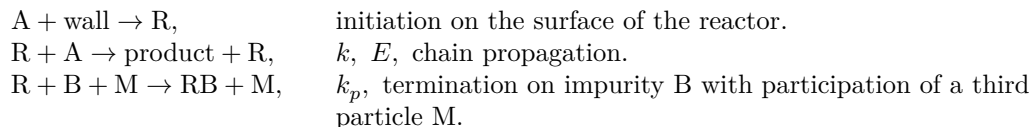
*(Presented by Academician V. N. Kondrat'ev, November 28, 1964)*

The condition of thermal self-ignition for a homogeneous gas reaction is determined by the relation <sup>(1, 2)</sup>

$$wq \frac{E}{RT_0^2} \sim \frac{a}{r_0^2},$$

where  $T_0$  is the temperature of the reactor wall;  $w$  is the reaction rate at  $T = T_0$ ;  $q$  and  $E$  are the heat and activation energy of the reaction;  $r_0$  is the linear dimension of the reactor, and  $a$  is a constant. It follows from this that, with increasing pressure, the conditions for ignition can only improve. Therefore it is considered that the upper limit of self-ignition can arise only in a chain branched reaction. However, one can simply indicate a concrete scheme of a chain unbranched reaction in which the existence of an upper limit is possible.

1. Let us consider the following hypothetical one-center scheme.



The distribution of radicals over the radius in a spherical reactor is determined by the diffusion equation

$$D\nabla_r^2[\text{R}] - k_p[\text{R}][\text{B}][\text{M}] = 0, \quad [\text{R}] = [\text{R}]_{r_0} \frac{r_0 \operatorname{sh} r/\rho}{r \operatorname{sh} r_0/\rho}, \quad (1)$$

where  $D$  is the diffusion coefficient of the radicals;  $\rho = 1/\sqrt{k_p[\text{B}][\text{M}]/D}$ , and  $r_0$  is the reactor radius.

In the case when  $r_0/\rho \gg 1$ ,  $[\text{R}]$  at the wall is well approximated by the exponential

$$[\mathbf{R}] \simeq [\mathbf{R}]_{r_0} e^{(r-r_0)/\rho}, \quad (2)$$

and the reaction rate near the reactor surface will be

$$w = k[\mathbf{R}]_{r_0} [\mathbf{A}] e^{(r-r_0)/\rho}. \quad (3)$$

Near the center (3) is certainly incorrect, but for solving the heat-conduction equation this is immaterial, provided only that the approximating function at  $r \sim 0$  is sufficiently small; (3) satisfies this requirement, and it may be used in solving the heat-conduction equation.

2. The temperature distribution over the reactor is given by the heat-conduction equation, in which, to simplify the calculation, we approximate the dependence of  $k$  on  $T$  by the first two terms of the expansion of  $k$  in powers of  $(T - T_0)$ :

$$\lambda \nabla_r^2 T + q k_{T_0} \left( 1 + \frac{E(T - T_0)}{RT_0^2} \right) [\mathbf{R}]_{r_0} [\mathbf{A}] e^{(r-r_0)/\rho} = 0; \quad (4)$$

$\lambda$  is the coefficient of thermal conductivity;  $q$  is the thermal effect of the reaction;  $T_0$  is the temperature of the reactor wall;  $k_{T_0}$  is the value of  $k$  at  $T - T_0$ .

The solution of (4) must be made subject to the boundary conditions

$$\text{a) } T = T_0 \quad \text{at } r = r_0; \quad \text{b) } T \text{ is bounded at } r = 0. \quad (5)$$

By the change of variables  $T = T_0 + u/r - RT_0^2/E$ ,  $x^2 = 4a\rho^2 e^{r/\rho}$ , where

$$a = q \frac{k_{T_0}}{\lambda} \frac{E}{RT_0^2} [\mathbf{A}] [\mathbf{R}]_{r_0} e^{-r_0/\rho}, \quad (4)$$

it is reduced to Bessel' s equation

$$x^2 u'' + x u' + x^2 u = 0.$$

The solution of (4) with conditions (5) is the function

$$T = T_0 + \frac{RT_0^2}{E} \left\{ \frac{r_0}{r} \frac{J_0(2\rho\sqrt{a} e^{r/2\rho}) - Y_0(2\rho\sqrt{a} e^{r/2\rho}) J_0(2\rho\sqrt{a}) / Y_0(2\rho\sqrt{a})}{J_0(2\rho\sqrt{a} e^{r/2\rho}) - Y_0(2\rho\sqrt{a} e^{r/2\rho}) J_0(2\rho\sqrt{a}) / Y_0(2\rho\sqrt{a})} - 1 \right\},$$

where  $J_0$  and  $Y_0$  are Bessel functions of the first and second kinds of zero order. For

$$J_0(2\rho\sqrt{a} e^{r_0/2\rho}) - Y_0(2\rho\sqrt{a} e^{r_0/2\rho})J_0(2\rho\sqrt{a})/Y_0(2\rho\sqrt{a}) = 0 \quad (6)$$

the temperature tends to  $\infty$ , and the relation between the parameters for which (6) is satisfied gives the self-ignition condition.

Owing to the smallness of  $2\rho\sqrt{a}$ ,  $Y_0(2\rho\sqrt{a})$  is a large negative quantity, so that the second term in (6) is small. Therefore one may use the approximate equation

$$J_0(2\rho\sqrt{a} e^{r_0/2\rho}) = 0, \quad (7)$$

whence we obtain the self-ignition condition in the form

$$\frac{D}{k_p[B][M]} q \frac{k_{T_0}}{\lambda} \frac{E}{RT_0^2} [A][R]_{r_0} \geq \frac{\mu_1^2}{4} \quad (8)$$

( $\mu_1$  is the first zero of  $J_0$ ).

3. The value of the concentration  $[R]_{r_0}$  near the wall is determined by the boundary condition

$$-D d[R]/dr|_{r=r_0} = \chi_2[R] - \chi_1[A], \quad (9)$$

where  $\chi_1[A]$  is the number of impacts of molecules  $A$  on 1 cm<sup>2</sup> of the reactor surface leading to the formation of radicals  $R$ ;  $\chi_2[R]$  is the number of impacts on 1 cm<sup>2</sup> of the surface in which radicals  $R$  are destroyed.

Using (2), from (9) we obtain  $[R]_{r_0} = \chi_1[A]/(\chi_2 + \sqrt{k_p[B][M]D})$ . Since  $[A] \sim p$ ,  $[B] \sim p$ ,  $[M] \sim p$ ,  $D \sim 1/p$ , then

$$[R]_{r_0} \sim p/(a + p^{1/2}) \quad (a \text{ is a constant}). \quad (10)$$

Substituting (10) into (8), it is easy to see that the left-hand side decreases with increasing pressure, so that the point of equality in (8) determines the upper limiting value of the pressure at which self-ignition of the reacting mixture still occurs.

4. Condition (8) is easily transformed to the form

$$w_{r_0} q \frac{E}{RT_0^2} \geq \frac{\mu_1^2}{4} \frac{\lambda}{\rho^2},$$

where  $w_{r_0}$  is the reaction rate near the wall.

In this form the self-ignition condition has the usual form, but instead of the reactor radius  $r_0$  there appears the thickness of the reaction zone  $\rho$ , which depends strongly, as  $p^{-3/2}$ , on the pressure. It is precisely this latter circumstance that is the physical cause of the appearance of the upper limit.

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## REFERENCES

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- <sup>2</sup> D. A. Frank-Kamenetskii, *Diffusion and Heat Transfer in Chemical Kinetics*, Moscow-Leningrad, 1947.

*Note: Figure translations are in progress. See original paper for figures.*

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