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Abstract

Full Text

MECHANICS

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ON THE THEORY OF FOUR-LINK MECHANISMS WITH TWO PRISMATIC PAIRS

Consider the question of the line envelopes of the coupler curves of a mechanism (Fig. 1) formed by two involute and two prismatic pairs with alternating arrangement. Let an arbitrary straight line $u - u$ be chosen in the plane of link 2. We shall find the instantaneous center of rotation P of link 2 and drop from the point P the perpendicular PM to the line $u - u$. The point M will belong to the curve that is the line envelope of the line $u - u$. Drop from the point A the perpendicular AF to the line $u - u$ and introduce the notation $AF = p$, $AE = p_1$, $AG = a$, and $EB = b$.

The equation for the family of straight lines $u - u$ will be

$$x \cos \theta + y \sin \theta = p. \quad (1)$$

or

$$x \cos(\theta_1 + \gamma) + y \sin(\theta_1 + \gamma) = p_1 \cos \gamma. \quad (2)$$

Take the partial derivative with respect to the parameter θ_1 of expression (2):

$$y \cos(\theta_1 + \gamma) - x \sin(\theta_1 + \gamma) = \frac{\partial p_1}{\partial \theta_1} \cos \gamma. \quad (3)$$

The segment p_1 will be equal to

$$p_1 = \frac{a - b \sin \theta_1}{\cos \theta_1}. \quad (4)$$

The partial derivative $\partial p_1 / \partial \theta_1 = \Psi$ will be equal to

$$\Psi = \frac{a \sin \theta_1 - b}{\cos^2 \theta_1}. \quad (5)$$

From equations (2) and (3) we obtain the parametric equations of the desired line-envelope curve:

$$\begin{aligned} x &= [p_1 \cos(\theta_1 + \gamma) - \Psi \sin(\theta_1 + \gamma)] \cos \gamma, \\ y &= [p_1 \sin(\theta_1 + \gamma) + \Psi \cos(\theta_1 + \gamma)] \cos \gamma, \end{aligned} \quad (6)$$

where the functions $p_1 = p_1(\theta_1)$ and $\Psi = \Psi(\theta_1)$ are determined by equations (4) and (5). If the angle $\gamma = 90^\circ$, then the line-envelope curve is transformed into the point A . For the angle $\gamma = 0$, the equations of the line envelope will have the form

$$\begin{aligned} x &= p_1 \cos \theta_1 - \Psi \sin \theta_1, \\ y &= p_1 \sin \theta_1 + \Psi \cos \theta_1. \end{aligned} \quad (7)$$

The locus of the point F will be the podaria of the line-envelope curve considered, if the point A is chosen as the pole of the podaria. The polar equation of this podaria will be

$$\rho = \frac{a - b \sin(\theta - \gamma)}{\cos(\theta - \gamma)} \cos \gamma. \quad (8)$$

Passing to a rectangular coordinate system, we obtain

$$(x^2 + y^2)[a \cos \gamma - (x \cos \gamma + y \sin \gamma)]^2 = b^2 \cos^2 \gamma (y \cos \gamma - x \sin \gamma)^2. \quad (9)$$

Consequently, the podaire will be an algebraic curve of the 4th order.

If the angle $\gamma = 0$, then the podaire will be the locus of points E (Fig. 1), and the equation of the podaire will be

$$(a - x)^2(x^2 + y^2) = b^2 y^2. \quad (10)$$

Equation (10) is the equation of the pan-kappa ⁽¹⁾. For $b = a$ we obtain the equation of an algebraic curve of the 3rd order

$$y^2 = \frac{a^2 x - (2a - x)x^2}{2a - x}. \quad (11)$$

Equation (11) is the equation of the right strophoid with point of self-intersection G . Indeed, passing to the coordinate system $x_1 G y_1$ (Fig. 1), we obtain the equation of the strophoid in the usual form

$$y_1^2 = \frac{a - x_1}{a + x_1} x_1^2. \quad (12)$$

From the mechanism shown in Fig. 1, the Lebeau mechanism ⁽²⁾, shown in Fig. 2, can be obtained. The parametric equations of the curve linearly enveloping

Fig. 1

Figure 1: Fig. 1

Fig. 2

Figure 2: Fig. 2

the straight line $u-u$ in the Lebeau mechanism can be obtained from equations (6), if in them one substitutes the values for p_1 and Ψ , respectively equal to $p_1 = b/\operatorname{tg} \theta_1$ and $\Psi = -b/\sin^2 \theta_1$:

Fig. 1

$$\begin{aligned} x &= b \cos \gamma \left[\frac{\cos \theta_1 \cos(\theta_1 + \gamma)}{\sin \theta_1} + \frac{\sin(\theta_1 + \gamma)}{\sin^2 \theta_1} \right], \\ y &= b \cos \gamma \left[\frac{\cos \theta_1 \sin(\theta_1 + \gamma)}{\sin \theta_1} - \frac{\cos(\theta_1 + \gamma)}{\sin^2 \theta_1} \right]. \end{aligned} \quad (13)$$

Fig. 2

For angle $\gamma = 90^\circ$ the linearly enveloping curve transforms into the point A . For angle $\gamma = 0$, the equations of the linearly enveloping curve will be

$$\begin{aligned} x &= b \left(\frac{1 + \cos^2 \theta_1}{\sin \theta_1} \right), \\ y &= b \frac{\cos \theta_1}{\operatorname{tg}^2 \theta_1}. \end{aligned} \quad (14)$$

The podaire of the curve described by equations (13), if point A is chosen as the pole, will be the locus of points F (Fig. 2).

The equation of this podaire in polar form will be

$$p = \frac{b \cos \gamma}{\operatorname{tg}(\theta - \gamma)}. \quad (15)$$

Passing to a rectangular coordinate system, we obtain the equation of the podaire in the form

$$(x^2 + y^2)(y - x \operatorname{tg} \gamma)^2 = b^2 \cos^2 \gamma (x + y \operatorname{tg} \gamma)^2. \quad (16)$$

If the angle $\gamma = 0$, then the pole curve will be the locus of points E , and the equation of the pole curve will be the equation of the “kappa” curve ⁽¹⁾

Fig. 3

Figure 3: Fig. 3

$$b^2x^2 = y^2(x^2 + y^2). \quad (17)$$

From the mechanism shown in Fig. 1, by taking $b = 0$, one can obtain the mechanism shown in Fig. 3.

The parametric equations of the curve linearly enveloping the straight line $u - u$ can be obtained from equations (6), if in them one substitutes the values for ρ_1 and Ψ , respectively equal to $\rho_1 = a / \cos \theta_1$ and $\Psi = a \sin \theta_1 / \cos^2 \theta_1$:

$$\begin{aligned} x &= \frac{a}{\cos^2 \theta_1} \cos(2\theta_1 + \gamma) \cos \gamma, \\ y &= \frac{a}{\cos^2 \theta_1} \sin(2\theta_1 + \gamma) \cos \gamma. \end{aligned} \quad (18)$$

Equations (18) are the equations of a parabola. Indeed, let us drop from point A to the straight line $u - u$ the perpendicular AF and connect point F with point G . Then, as was shown earlier by us ⁽¹⁾, the mechanism under consideration can be replaced by an equivalent mechanism (Fig. 3), in which link $2'$ enters into a prismatic pair with slider $1'$, rotating about the axis A , and into a revolute pair with slider $3'$, sliding along the axis FG . The straight line $u' - u'$, rigidly connected with link $2'$ and forming an angle of 90° with the direction AF , will always coincide with the straight line $u - u$. The parabola that is the curve linearly enveloping the straight line $u - u$ or $u' - u'$ will have, as its vertex, the point O —the foot of the perpendicular dropped from point A onto the direction FG —and, as its focus, point A . The pole curve of the parabola defined by equations (18) is the straight line FG .

Fig. 3

If we take the angle $\gamma = 0$, then the curve linearly enveloping the straight line $u - u$ will be a parabola with focus at point A and vertex at point G . The equation of this parabola will be

$$y^2 = 4a(a - x) \quad (19)$$

and its pole curve will be the straight line BG . If point A is chosen as the pole, then the pole curve of this parabola will be the straight line FG . The latter, in particular, proves the kinematic equivalence of the mechanism AF to the mechanism AB .

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REFERENCES

1. I. I. Artobolevsky, *Theory of Mechanisms for the Reproduction of Plane Curves*, Publishing House of the Academy of Sciences of the USSR, 1959.
2. V. Lebeau, *Mémoires de la Soc. Roy. de Sci. de Liège*, sér. 3, 5, 1904.

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