



Soviet-era science, translated into English

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1958

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Abstract

Full Text

THEORY OF ELASTICITY

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STRESSES IN A SYMMETRICALLY HEATED SPHERICAL SHELL WHOSE MECHANICAL PROPERTIES DEPEND ON TIME AND TEMPERATURE

(Presented by Academician S. L. Sobolev, 13 I 1958)

1. Let a closed spherical shell be given, with external and internal radii a_1 and a_2 , free of external forces and initial stresses, at a uniformly distributed temperature. Suppose that, beginning at some moment, the temperature in the shell becomes nonuniformly distributed, and assume that the temperature $T = T(r, t)$ is known. Then stresses and strains of a definite magnitude will arise in it.

We determine the radial displacement $u(r, t)$ and the stresses arising in the body in question in the case where the Lamé coefficients λ and μ and the relaxation characteristics depend on temperature, and also taking into account aging of the material, i.e., the variability of λ and μ with time t .

Generalizing in the appropriate way the Volterra dependences ⁽¹⁾, we write the stress components in spherical coordinates

$$\begin{aligned} \sigma_r &= \lambda\theta + 2\mu \frac{\partial u}{\partial r} - \int_{t_0}^t \left[\varphi(t, \tau; r)\theta + 2\psi(t, \tau; r) \frac{\partial u}{\partial r} \right] d\tau - \alpha\beta T, \\ \sigma_\theta = \sigma_\varphi &= \lambda\theta + 2\mu \frac{u}{r} - \int_{t_0}^t \left[\varphi(t, \tau; r)\theta + 2\psi(t, \tau; r) \frac{u}{r} \right] d\tau - \alpha\beta T, \end{aligned} \quad (1)$$

where $\theta(r, t)$ is the volume expansion; $\varphi(t, \tau; r)$ and $\psi(t, \tau; r)$ are the relaxation kernels; λ , μ , and $\beta = 3\lambda + 2\mu$, as well as the coefficient of linear expansion α , depend on the coordinate r and time t , since, by assumption, the temperature of the shell is considered a known function of r and t .

Substituting σ_r , $\sigma_\theta = \sigma_\varphi$ from (1) into the usual equilibrium equation, we obtain the initial integro-differential equation, which we present in the form

$$\begin{aligned} \frac{\partial}{\partial r} \left[(\lambda + 2\mu) \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 u) \right] - \frac{4}{r} \frac{\partial \mu}{\partial r} u - \frac{\partial}{\partial r} (\alpha \beta T) + \frac{4}{r} \int_{t_0}^t \frac{\partial \psi(t, \tau, r)}{\partial r} u(r, \tau) d\tau = \\ = \int_{t_0}^t \frac{\partial}{\partial r} \left\{ [\varphi_1(t, \tau; r) + 2\psi(t, \tau; r)] \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 u) \right\} d\tau. \end{aligned} \quad (2)$$

Put

$$\frac{\partial}{\partial r} \left[\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 u) \right] = z(r, t). \quad (3)$$

From (3) it follows that

$$u(r, t) = \frac{1}{3r^2} \int_{a_1}^r (r^3 - \rho^3) z(\rho, t) d\rho + c_1(t)r + r^{-2}c_2(t). \quad (4)$$

where c_1 and c_2 are arbitrary functions of time, which are determined from the boundary conditions

$$\left\{ \lambda \left(\frac{\partial u}{\partial r} + \frac{2u}{r} \right) + 2\mu \frac{\partial u}{\partial r} - \alpha \beta T - \int_{t_0}^t \left[\varphi(t, \tau; r) \left(\frac{\partial u}{\partial r} + \frac{2u}{r} \right) + 2\psi(t, \tau; r) \frac{\partial u}{\partial r} \right] d\tau \right\}_{r=a_k} = 0 \quad (5)$$

($k = 1, 2$) after $z(r, t)$ has been found.

Substituting (3) and (4) into equation (2), after the corresponding transformations we obtain the mixed two-dimensional integral equation

$$\begin{aligned} z(r, t) + \int_{a_1}^r K_1(t; r, \rho) z(\rho, t) d\rho - \int_{t_0}^t K_2(t, \tau; r) z(r, \tau) d\tau = \\ = \int_{t_0}^t \int_{a_1}^r K_3(t, \tau; r, \rho) z(\rho, \tau) d\rho d\tau + f(r, t, c_1, c_2), \end{aligned} \quad (6)$$

where

$$\begin{aligned} K_1(t; r, \rho) &= \frac{1}{\lambda + 2\mu} \left[\frac{\partial}{\partial r} (\lambda + 2\mu) - \frac{4(r^3 - \rho^3)}{3r^3} \frac{\partial \mu}{\partial r} \right], \\ K_2(t, \tau; r) &= \frac{\varphi(t, \tau; r) + 2\psi(t, \tau; r)}{\lambda + 2\mu}, \end{aligned}$$

$$K_3(t, \tau; r, \rho) = \frac{1}{\lambda + 2\mu} \left\{ \frac{\partial}{\partial r} [\varphi(t, \tau; r) + 2\psi(t, \tau; r)] - \frac{4(r^3 - \rho^3)}{3r^3} \frac{\partial \psi(t, \tau; r)}{\partial r} \right\},$$

$$f(r, t; c_1, c_2) = \frac{1}{\lambda + 2\mu} \left\{ \frac{4}{r} \left(c_1 r + \frac{c_2}{r^2} \right) \frac{\partial \mu}{\partial r} - \frac{4}{r} \int_{t_0}^t \left(c_1 r + \frac{c_2}{r^2} \right) \frac{\partial \psi(t, \tau; r)}{\partial r} d\tau \right. \\ \left. - 3c_1 \frac{\partial}{\partial r} (\lambda + 2\mu) + 3 \int_{t_0}^t c_1(\tau) \frac{\partial}{\partial r} [\varphi(t, \tau; r) + 2\psi(t, \tau; r)] d\tau \right\}.$$

Determining z from equation (6) and then substituting into (4), after the corresponding transformations we obtain the formula for the displacement

$$u = c_1 A_1(t, r) - \int_{t_0}^t [A_2(t, \tau; r) c_1(\tau) - A_3(t, \tau; r) c_2(\tau)] d\tau + c_2 r^{-2}, \quad (7)$$

where

$$A_1(t, r) = r + \frac{1}{3r^2} \int_{a_1}^r \frac{D(t; r, \rho)}{\lambda + 2\mu} \left[4 \frac{\partial \mu}{\partial \rho} - 3 \frac{\partial}{\partial \rho} (\lambda + 2\mu) \right] d\rho,$$

$$D(t; r, \rho) = r^3 - \rho^3 - \int_{\rho}^r (r^3 - \rho_1^3) R_1(t; \rho_1, \rho) d\rho_1,$$

$$A_2(t, \tau; r) = \frac{1}{3r^2} \int_{a_1}^r \frac{D(t; r, \rho)}{\lambda + 2\mu} \left[4 \frac{\partial \psi(t, \tau; r)}{\partial \rho} - 3 \frac{\partial}{\partial \rho} (\varphi(t, \tau; r) + 2\psi(t, \tau; r)) \right] d\rho,$$

$$A_3(t, \tau; r) = \frac{4}{3r^2} \int_{a_1}^r \frac{\rho^{-3}}{\lambda + 2\mu} \left[E(t, \tau; r, \rho) \frac{\partial \mu}{\partial \rho} - \int_{\tau}^t E(t, \tau_1; r, \rho) \frac{\partial \psi(\tau_1, \tau; \rho)}{\partial \rho} d\tau_1 \right],$$

$$E(t, \tau; r, \rho) = (r^3 - \rho^3) R_2(t, \tau; \rho) + \int_{\rho}^r (r^3 - \rho_1^3) R_3(t, \tau; \rho_1, \rho) d\rho_1,$$

$$R_3(t, \tau; r, \rho) = R(t, \tau; r, \rho) + \int_{\tau}^t R_2(t, \tau_1; r) R(\tau_1, \tau; r, \rho) d\tau_1 - \\ - \int_{\rho}^r R_1(t; r, \rho_1) R(\tau_1, \tau; \rho_1, \rho) d\rho_1 -$$

$$- \int_{\tau_1}^t d\tau_1 \int_{\rho}^r R_1(\tau_1; r, \rho_1) R_2(t, \tau_1; \rho_1) R(\tau_1, \tau; \rho_1, \rho) d\rho_1;$$

$R_1(t; r, \rho)$ and $R_2(t, \tau; r)$ are the resolvents of the kernels $K_1(t; r, \rho)$ and $K_2(t, \tau; r)$, respectively; $R(t, \tau; r, \rho)$ is the resolvent of the kernel

$$\left[Q(t, \tau; r, \rho) + \int_{\tau}^t Q(t, \tau_1; r, \rho) R_2(\tau_1, \tau; \rho) d\tau_1 \right];$$

$$Q(t, \tau; r, \rho) = K_3(t, \tau; r, \rho) - K_2(t, \tau; r) R_1(\tau; r, \rho) - \int_{\rho}^r K_3(t, \tau; r, \rho_1) R_1(\tau; \rho_1, \rho) d\rho_1.$$

The functions $c_1(t)$ and $c_2(t)$ appearing in (7) are determined from the system of ordinary integral equations

$$\sum_{i=1}^2 \left[\alpha_{ik} c_k(t) - \int_{t_0}^t \Phi_{ik}(t, \tau) c_k(\tau) d\tau \right] = F_k, \quad (8)$$

where

$$\alpha_{ik} = \left\{ \frac{1 - (-1)^i}{2} \left[(\lambda + 2\mu) \frac{\partial A_1}{\partial r} + 2\lambda \frac{A}{r} \right] - 2\mu \frac{(-1)^i + 1}{r^3} \right\}_{r=a_k} \quad (i, k = 1, 2);$$

$$F_k = \alpha_k \beta_{kT} k; \quad \Phi_{ik}(t, \tau) = \left\{ \frac{1 - (-1)^i}{2} (\varphi + 2\psi) \frac{\partial A_1}{\partial r} - 2\psi \frac{(-1)^i + 1}{r^3} + \right.$$

$$\left. + \frac{(-1)^k + 1}{2} \left[(\lambda + 2\mu) \frac{\partial A_{i+1}}{\partial r} - \frac{2\lambda}{r} A_{i+1} - \int_{\tau}^t \left((\varphi + 2\psi)_{\tau_1} \frac{\partial A_{i+1}}{\partial r} + \frac{2\varphi}{r} A_{i+1} \right) d\tau_1 \right] \right\}_{r=a_k}.$$

System (8) has a unique solution.

From the first equation of system (8) it follows that

$$c_1(t) = \frac{F_1}{a_{11}} + \int_{t_0}^t \frac{H(t, \tau)}{a_{11}(\tau)} F_1(\tau) d\tau - \frac{a_{21}}{a_{11}} c_2(t) + \int_{t_0}^t H_1(t, \tau) c_2(\tau) d\tau, \quad (9)$$

where

$$H_1(t, \tau) = \alpha_{11}^{-1}(\tau) \left[\Phi_{21}(t, \tau) - \alpha_{21}H(t, \tau) + \int_{\tau}^t H(t, s)\Phi_{21}(s, \tau) ds \right],$$

$H(t, \tau)$ is the resolvent of the kernel $\Phi_{11}(t, \tau)/\alpha_{11}$.

Substituting (9) into the second equation of system (8), we obtain an integral equation with one unknown c_2 . Determining c_2 from the equation thus obtained and then again using (9), we obtain formulas determining c_k .

Knowing the displacement u , it is easy to determine σ_r , $\sigma_\theta = \sigma_\varphi$.

2. The obtained results are considerably simplified if it is assumed that $\lambda = \mu = \lambda_0 e^{-mT}$, $\varphi(t, \tau; r) = \psi(t, \tau; r) = \varphi_0(t, \tau) e^{-mT}$, where m is a constant for the given material; λ_0 and $\varphi_0(t, \tau)$ are the Lamé coefficient and the relaxation kernel at $T = 0$; the temperature T still depends on r and t .

The decrease of the physico-mechanical characteristics is proportional to many... for a viscosity that decreases exponentially with increasing temperature, is confirmed experimentally (2).

The substitution (3) leads to an ordinary integral equation with respect to z , with a fairly simple kernel.

As a result we shall have

$$u(r, t) = \int_{a_1}^r N_1(t; r, \rho) T_*(\rho, t) d\rho + c_1 \left[r + \frac{5m}{3} \int_a^r N_1(t; r, \rho) \frac{\partial T}{\partial \rho} d\rho \right] + c_2 \left[\frac{1}{r^2} - \frac{4m}{3} \int_{a_1}^r N_1(t; r, \rho) \frac{1}{\rho^3} \frac{\partial T}{\partial \rho} d\rho \right], \quad T_* = T_1 + \int_{t_0}^t P(t, \tau) T_1 d\tau, \quad (10)$$

$$N_1(t; r, \rho) = \frac{1}{3r^2} \left[r^3 - \rho^3 + \int_{\rho}^r (r^3 - \rho_1^3) N(t; \rho_1, \rho) d\rho_1 \right];$$

$P(t, \tau)$ and $N(t; r, \rho)$ are the resolvents of the kernels $\frac{\varphi_0(t, \tau)}{\lambda_0}$ and

$$\frac{m}{9} \left(5 + \frac{4\rho^3}{r^3} \right) \frac{\partial T}{\partial r},$$

respectively;

$$T_1 = 5 \left[\frac{\partial}{\partial r} (\alpha T) - m\alpha T \frac{\partial T}{\partial r} \right].$$

The functions $c_1(t)$ and $c_2(t)$ appearing in (10) are expressed by the formulas

$$\begin{aligned}
 c_1 &= \frac{a_1^3 B_2 \Phi_{a_1} - a_2^3 \Phi_{a_2}}{a_2^3 B_1 - a_1^2 B_2}, & c_2 &= \frac{5a_1^3 a_2^3 (\Phi_{a_2} - B_1 \Phi_{a_1})}{4(a_2^3 B_1 - a_1^2 B_2)}, \\
 B_1 &= 1 + \frac{m}{3} \int_{a_1}^{a_2} \frac{\partial T}{\partial \rho} \left[\frac{\partial N_1(t; r, \rho)}{\partial r} + \frac{N_1(t; r, \rho)}{a_2} \right]_{r=a_2} d\rho, & (11) \\
 B_2 &= 1 + m a_2^3 \int_{a_1}^{a_2} \frac{1}{\rho^3} \frac{\partial T}{\partial \rho} \left[\frac{\partial N_1(t; r, \rho)}{\partial r} + \frac{2N_1(t; r, \rho)}{3a_2} \right]_{r=a_2} d\rho;
 \end{aligned}$$

Φ_{a_1} and Φ_{a_2} are the values of the function

$$\Phi(r, t) = \alpha T + \int_{t_0}^t P(t, \tau) \alpha T d\tau$$

at $r = a_1$ and $r = a_2$, respectively.

Formulas (11) are obtained as the result of solving the system of algebraic equations formed by using the boundary conditions (5).

As an illustration, let us consider a steel hollow ball with the following parameters: $m = 0.0008 \text{ deg}^{-1}$ (according to the experimental data of Zaikov ⁽²⁾), $a_1 = 30 \text{ cm}$, $a_2 = 33 \text{ cm}$, $T = 9900r^{-1} + 670$, $T(a_1) = 1000^\circ$, $T(a_2) = 970^\circ$, $\alpha = 11 \cdot 10^{-6} \text{ deg}^{-1}$,

$$P(s) = 0.0175(s/33)^{0.75} \exp\left(-\sqrt[4]{s/33}\right)$$

(according to ⁽³⁾). Approximately we obtain

$$u = (0.1165 - 0.00762 \exp(-\sqrt[4]{t/33}))(0.9853 - 0.04097r - 17.85r^{-1} - 525.5r^{-2} - 2253r^{-3} + 1898r^{-4} + 46r^{-3} \ln r + 3.5)$$

In particular, for example, the steady-state value of the strain at the outer surface will be

$$\varepsilon = 0.00507.$$

In conclusion I express my gratitude to Yu. A. Ponomarenko and L. I. Paikova for assistance in the computations connected with the reduction to concrete examples.

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Received
31 V 1957

CITED LITERATURE

¹ V. Volterra, *Theory of Functionals and of Int.-differential Equations*, London, 1931.

² M. A. Zaikov, *ZhTF*, 18, no. 6 (1948).

³ A. P. Bronskii, *Prikl. matem. i mekh.*, 5, no. 1 (1941).

Note: Figure translations are in progress. See original paper for figures.

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