

Doubling the power efficiency of radioluminescent batteries via tuning the optical field

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Abstract

Radioluminescent (RL) batteries, offering exceptional energy density and extended operational lifetime, hold significant promise for applications in remote and extreme environments such as aerospace and deep-sea exploration. However, their widespread applications have been hindered by low energy conversion efficiency, primarily stemming from the poor optical outcoupling. In this work, we successfully doubled the efficiency of $\text{Cs}_3\text{Cu}_2\text{I}_5$: Tl-based X-ray RL batteries through systematic optical field engineering. A reflective film was applied on the top and side surfaces of the scintillator to minimize light losses. An optocoupler adhesive was adopted to realize refractive index matching between the scintillator and the photovoltaic cell, which not only shortens the light propagation path within the scintillator but also minimizes selfabsorption losses. As a result, the optical coupling efficiency was improved from 22.9% to 51.0%, leading to a 133.7% enhancement in overall device performance. The optimized battery achieves a power conversion efficiency of 2.15% and an output power density of $12.9 \mu\text{W}/\text{cm}^2$. This study not only underscores the critical role of optical field management in advancing RL battery technology but also provides a strategic pathway for unlocking the full potential of RL batteries.

Full Text

Preamble

Doubling the power efficiency of radioluminescent batteries via tuning the optical field
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Radioluminescent (RL) batteries, offering exceptional energy density and

extended operational lifetime, hold significant promise for applications in remote and extreme environments such as aerospace and deep-sea exploration. However, their widespread applications have been hindered by low energy conversion efficiency, primarily stemming from the poor optical outcoupling. In this work, we successfully doubled the efficiency of β -based X-ray RL batteries through systematic optical field engineering. A reflective film was applied on the top and side surfaces of the scintillator to minimize light losses. An optocoupler adhesive was adopted to realize refractive index matching between the scintillator and the photovoltaic cell, which not only shortens the light propagation path within the scintillator but also minimizes self-absorption losses. As a result, the optical coupling efficiency was improved from 22.9% to 51.0%, leading to a 133.7% enhancement in overall device performance. The optimized battery achieves a power conversion efficiency of 2.15% and an output power density of 12.9 W/m². This study not only underscores the critical role of optical field management in advancing RL battery technology but also provides a strategic pathway for unlocking the full potential of RL batteries.

Keywords

Isotope battery, Radioluminescent battery, Scintillator, Outcoupling efficiency, Power conversion efficiency

INTRODUCTION

Radioluminescent (RL) photovoltaic batteries have recently garnered increasing research attention due to their

unique advantages, including extremely high energy density, 4

and ultralong lifetime [These attributes make them

particularly attractive for powering micro-electromechanical 6

systems (MEMS) and aerospace electronics in extreme en- 7

vironments where reliability and longevity are of paramount importance[]. However, unlike direct-conversion radio- voltaic batteries[], RL batteries operate via an indirect

energy conversion scheme. The ionizing radiation is first con- 11

verted into visible light within a scintillator, which is then

harvested by a photovoltaic unit to generate electricity. This 13

two-step process inherently introduces additional energy loss pathways, placing RL batteries at a comparative disadvantage in terms of overall energy conversion efficiency[Therefore, improving the energy conversion efficiency has emerged as the most critical research priority for advancing the practical application of RL battery.

Previous efforts to enhance the overall conversion efficiency of RL batteries have focused on optimizing the scintillator, primarily through two strategies: improving the intrinsic radio-luminescence efficiency of scintillator materials and enhancing the light collection efficiency[1]. As for novel scintillator materials, zero-dimensional copper-based halides, particularly Cu_2O , have emerged as promising candidates for RL battery applications due to their high light yield[2]. Zeng et al. introduced Cu_2O -doped scintillators, achieving a light yield of 67,000 photons/MeV and demonstrating an output power density of 0.9 $\mu\text{W}/\text{cm}^2$ in a prototype RL battery[3]. Subsequently, Ouyang et al. reported a high-performance RL nuclear battery based on ultrabright single crystal scintillators, attaining an output power of 0.9 $\mu\text{W}/\text{cm}^2$, which surpassed the performance of batteries employing conventional ZnS:Ag and LYSO:Ce scintillators[4].

Parallel efforts have been directed toward improving light collection efficiency. Xu et al. conducted systematic investigations on the scintillator-photovoltaic interface, demonstrating that a silver nanosphere array deposited on the photovoltaic cell surface enhances forward scattering of RL photons, thereby increasing the light absorption by up to 43.66% and boosting electrical output by 44.91%[5]. They also proposed incorporating a nanosphere coating within the fluorescent layer to address weak radioluminescence, achieving a 51.59% improvement in maximum output power[6]. Separately, San et al. explored the role of reflective layers on the scintillator surface, systematically investigating the effect of reflective layer type and thickness. Their results showed that a 100 nm thick Ag film yielded a 52.6% enhancement in RL battery efficiency[7]. Overall, all studies focusing on the optimization of scintillators in RL batteries have demonstrated promising results.

Our previous work has theoretically identified that the energy conversion efficiency within the scintillator remains the primary bottleneck in RL battery performance[8]. Moreover, among the various loss mechanisms, the optical outcoupling efficiency of the scintillator emerges as the most critical factor requiring immediate improvement. However, no systematic investigation has been done to specifically address and improve the optical outcoupling efficiency in RL batteries. In particular, the mechanisms by which the reflection layer and the scintillator-photovoltaic interface affect the optical losses within the scintillator remain poorly understood. The details of optical field regulation require further targeted optimization to maximize the overall efficiency

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layer and the scintillator-photovoltaic interface affect the optical losses within the scintillator remain poorly understood.

The details of optical field regulation require further targeted

single crystal scintillator, inset: photograph of the single crystal scintillator; (b) UV-vis absorption (black line) and PL emission (red line) spectra of the single crystal scintillator; (c) RL spectra of and BGO scintillator under the radiation of an X-ray tube biased at 20 kV. optimization to maximize the overall efficiency

enhancement of RL batteries. To address this gap, this study establishes a comprehensive Monte Carlo multi-physics coupling model for the most promising -based X-ray RL bat- tery. This model enables quantitative analysis of the optical outcoupling efficiency and systematically clarifies the loss

mitigation mechanisms enabled by the reflection layer and the 72

optical outcoupling layer. Through the synergistic optimiza- tion of self-absorption losses and surface optical losses, we successfully achieve a doubling of the battery' s overall en- ergy conversion efficiency.

MATERIALS AND METHODS Optical and RL properties of The Tl-doped single crystal was selected as the scintillator material in this study for the X-ray RL battery, owing to its high light yield and low self-absorption, as re- ported in previous paper. A systematic investigation of the optical and RL properties of the scintil- lator including light yield, refractive index, and absorption coefficient, was conducted to obtain all the key optical pa- rameters of the scintillators as inputs for the Geant4 simula- tion model. Fig. (a) presents the transmission and reflection spectra of a 0.6 mm-thick, 3.5 mm-radius single-crystal scintilla- tor. The scintillator exhibits high trans- mittance, reaching approximately 85% across the entire visi- ble spectrum. Based on the average transmittance, the refrac- tive index was determined to be

- 1.
2. A decline in trans- mittance is observed at wavelengths below 350 nm, which is attributed to the interband absorption. Furthermore, the re- flectance remains around 3% within the 300–800 nm range,

indicating a smooth and optically uniform surface.

Based 96

on the absorption spectrum, the absorption coefficient of scintillator was calculated to be 0.089 and photoluminescence (PL) emission (red line) spectra of single-crystal scintillator, with an excita- tion wavelength of 350 nm. The scintillator exhibits a strong absorption peak at approximately 350 nm and a broad green emission band ranging from 400 nm to 750 nm, centered at around 510 nm with a full width at half maximum (FWHM) of 110 nm. The observed Stokes shift is about 160 nm, indi- cating a low self-absorption characteristic, which meets per- fectly the material requirements of X-ray RL batteries. and a BGO scintillator under X-ray irradi- tion from a tube operated at 20 kV. The RL spectrum of the scintillator exhibits the same spectral range and peak position as its photoluminescence (PL) spectrum.

At this tube voltage, both scintillators fully absorb the inci- dent X-ray energy. The scintillator demon-

strates significantly higher RL intensity compared to the BGO 117

scintillator, which has a standard light yield of 8000 pho- tons/MeV. Accord- ingly, the light yield of the scintillator is calculated to be 50,000 photons/MeV.

Through the systematic characterization of the optical and RL properties of , as summarized in Fig. , key parameters including light yield, refractive index, and absorption coefficient have been determined and can be directly utilized as inputs for the Geant4 simulation model.

Establishment of the Geant4 Monte Carlo model The physical processes of light emission and outcoupling in the scintillator of the RL battery are schematically illustrated in Fig. (a). The X-rays incident into the scintillator

and excite the free electrons, with the cost of the ionized energy

of the scintillator. The free electrons relax to the ground states of the conduction band of the scintillator and then hop to the excited energy levels of the doped activators, which will radiatively recombine and emit light. The optical photons will either be self-absorbed or escape from all surfaces of the scintillator, among which only the part emitted from the

bottom surface can be outcoupled into the photovoltaic unit

and converted into electrons. The light emission and propagation processes are illustrated in the left and right part of

- (b) Energy dissipation process of optical photons in RL battery simulated using the Geant4 Monte Carlo model, where white lines stand for the trajectory of X-rays, green lines for optical photons, and yellow spots for the energy loss events. The energy loss of the RL process strongly depends on the properties of the scintillators, which is not in the scope of this work. This work mainly focuses on the dominating factors which is not related to the properties of scintillators in the RL battery.

The ratio of photon energy dissipated into each mode can be calculated using the Geant4 simulation. The RL battery model incorporating both the radiation and optical fields is presented in Fig.

The X-ray spectrum emitted from the X-ray tube was calculated by Spekpy and used to mimic the spectrum of the X-ray source in the Monte Carlo simulation. 10000 X-ray photons were used in each simulation.

The electromagnetic interactions between X-rays and scintillators were simulated using a custom model that accounts into all the key physical processes, including the photoelectric effect, Compton scattering, Rayleigh scattering, and electron pair production. The built-in model in Geant4 software registering the optical properties of the scintillator and the

photovoltaic unit (including light yield, refractive index, and

absorption coefficient etc.) is employed to simulate all the

optical process. The unified model is chosen to as the optical

boundary conditions and used to simulate all optical surfaces. As illustrated in Fig. (b), white lines stand for the trajectory of X-rays and green lines trace

the paths of optical photons generated within the scintillator. Photons either undergo the total internal reflection (TIR) or transmit into the

PV unit (representing coupled light) or escape to the atmosphere

sphere (representing light leakage), when encounter the surfaces, i.

- e. the optical boundaries. The scattering processes are not considered in the simulation, since the scintillator used in this study is transparent single-crystal (SC). Part of the photons can also be absorbed at the defects, which is presented as yellow spots for the energy loss events. As shown in the simulation, the optical photons will either be self-absorbed or escape from all surfaces of the scintillator, among which only the part emitted from the bottom surface can be outcoupled

into the photovoltaic unit and converted into electrons.

Validation of the model To verify the accuracy of the established multi-physics coupling model, CsI:Tl single crystal scintillators were employed for experimental validation. Fig. (a) presents five CsI:Tl samples with thicknesses ranging from 0.2 mm to 1.0 mm. These scintillators with varying thicknesses will exhibit differences in X-ray absorption and RL self-absorption, making them suitable for benchmarking the model predictions. The transmission spectra of the five CsI:Tl scintillators are shown in Fig. (a), revealing reduced optical transparency with increasing thickness. Based on these transmission curves, the self-absorption coefficient of the CsI:Tl scintillator material was extracted by fitting the linear relationship between $\ln(T)$ and thickness. The fitting results, displayed in Fig. (b), yield a self-absorption coefficient of $\mu_{sa} = 0.012 \text{ mm}^{-1}$. To investigate the RL response of CsI:Tl scintillators with varying thicknesses, measurements were performed under X-ray irradiation at different tube voltages, with the results presented in Fig. (c).

At low tube voltages, the RL intensity of the CsI:Tl scintillator increases with thickness. As the tube voltage rises, however, the RL intensity exhibits a trend of first increasing and then decreasing with thickness. Specifically, at a tube voltage of 30 kV, the scintillator with a thickness of 0.4 mm yields the highest RL intensity, whereas at 40 kV and 50 kV, the maximum fluorescence intensity is observed for the 0.6 mm thick sample. This trend reflects the trade-off between X-ray absorption and light self-absorption: increasing the scintillator thickness enhances X-ray absorption but also leads to greater optical losses due to self-absorption. At lower tube voltages, the effect of thickness on X-ray absorption is less pronounced. At higher voltages, the increased penetration depth results in reduced RL intensity for thinner scintillators. Fig. (d) displays the corresponding simulation results obtained from the theoretical

CsI:Tl single crystal scintillators; (c) Measured and (d) simulated changes in radioluminescence intensity of CsI:Tl scintillators with different thicknesses under different X-ray tube voltages. The modeled trends are in excellent agreement with the experimental observations, and the normalized RL inten-

sity variations closely match the measured data. These findings confirm the reliability and predictive capability of the developed model.

RESULTS AND DISCUSSIONS Optical loss modes in X-ray Battery setup for the X-ray RL battery. An X-ray tube with a tungsten target (Oxford, Apogee 5500) was employed to mimic a low-energy X-ray radioactive source, owing to its advantageous features such as a steerable irradiation area, adjustable

X-ray flux, and minimal radiation protection requirements. 224

scintillator and a GaInP photovoltaic

unit, with a bandgap of 1.84 eV, were positioned directly beneath the X-ray tube. The size of the GaInP PV unit is one 226

centimeter square, which is larger than the scintillator. In order to avoid the impact of direct X-ray irradiation on the GaInP PV unit, a collimator was used to ensure 230

that the X-ray irradiation area is on the scintillator. In order to maximize the output power of the X-ray RL battery, the tube was operated at the highest tube voltage of 50 kV. The spectrum of X-ray with 50 kV tube voltage was measured using a SDD detector as shown in Fig. (a). The spectrum shows the L-series characteristic peaks of tungsten at 8.4 keV, 9.7 keV and 11.3 keV, and the average energy of X-rays is 14.5 keV. The measured X-ray spectrum was used to calculate the energy deposition profile and the absorbed energy ratio within the scintillator, as illustrated in Fig. (b). The energy deposition exhibits an exponential decay profile, and it was determined that a 0.6 mm-thick scintillator absorbs 96.4% of the incident X-ray energy.

The inset in Fig. (c) illustrates the spectral matching between the external quantum efficiency (EQE) of the GaInP photovoltaic unit and the radioluminescence (RL) spectrum 247 of the scintillator. The cutoff edge of the GaInP EQE spectrum is slightly lower than that of the RL emission from the scintillator. In accordance with the method

for optimizing the bandgap of photovoltaic units reported 251 in our previous work, the 1.84 eV GaInP cell represents

single crystal scintillator using an X-ray tube; (b) Energy deposition profile and deposited energy ratio in scintillators under the radiation of an X-ray tube biased at 50 kV, where 96.4% of the total energy is deposited in 0.6 mm; (c) Current density-voltage (J-V) curves of X-ray RL battery based on scintillator and GaInP photovoltaic unit under the radiation of an X-ray tube biased at 50 kV and with a tube current of 1mA; Inset: Spectral matching between the RL spectrum of scintillator and EQEs of GaInP photovoltaic unit with a bandgap

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of 1.84 eV; (d) Quantitative analysis of different optical loss mechanisms in the battery. a balance between photon absorption and output voltage, thereby maximizing the power output of the X-ray RL battery. istics of the X-ray RL battery, comprising the

scintillator and the GaInP photovoltaic unit, under X-ray ir- 257

radiation at 50 kV and 1.0 mA. The device exhibits a short- circuit current density () of 9.6 , an open-circuit voltage () of 0.834 V, a fill factor (FF) of 68.5%, a max- imum output power density () of 5.51 , and an energy conversion efficiency () of 0.92%.

The Geant4 model as shown in Section 2.2 was employed to quantitatively analyze the different optical loss mecha-

nisms in the battery without optical field tuning, utilizing the 265

optical properties obtained from Fig. . The results are pre- sented in Fig. (d). As clearly indicated, only 22.9% of the

generated light is outcoupled into the photovoltaic unit, while 268

33.4% is self-absorbed within the scintilla-

tor. The remaining 42.8% escapes through the top surface 270

(39.2%) and the side surfaces (4.5%). The proportion of self- absorbed photons is determined by both the light path length and the absorption coefficient of the scintillator. Once the scintillator material is selected, this loss can only be reduced

by minimizing the total optical path length. An outcoupling 275

efficiency of 22.9% implies that roughly one in four photons

reach the photovoltaic unit. This efficiency can be improved 277

by mitigating top and side surface losses and enhancing light extraction at the bottom interface.

Reflection film to reduce the light leakage in scintillators In order to mitigate optical losses from the top and side surfaces of the scintillator, three types of re- flective films were evaluated: a 20 thick aluminum foil (#1), a 20 Al-coated PET film with a 1 aluminum

layer (#2), and a 65 μm thick organic reflective film (#3, 285

ESR, 3M). The inset in the figure shows the photograph of these three kinds of reflection films. Aluminum foil was se- lected as a commonly used reflector in RL batteries due to its high reflectivity. However, to reduce the energy absorption of

aluminum foil (#1), a 20 Al-coated PET film (#2), and a 65 Organic Reflection film (#3); (b) Energy deposition profiles in three kinds of reflection layers un-

der the radiation of an X-ray tube biased at 50 kV; (c) Current density-voltage (J-V) characteristic curves of the RL battery with no addition reflection layer and three kinds of reflection layers measured under the radiation of an X-ray tube biased at 50 kV and with a tube current of 1mA; (d) Quantitative analysis of different optical loss mechanisms in the four battery configurations; (e) Comparison of the measured short-circuit currents and the calculated incident light intensities of the batteries with four configurations.

X-rays, which is influenced by the effective atomic number, an Al-coated PET film was also investigated, as PET offers a lower effective atomic number compared to aluminum. Fur-

thermore, a fully organic reflective film was included to min- 293

imize both X-ray energy loss and surface plasmon resonance (SPR)-induced optical loss. Fig. (a) displays the reflection

spectra of the three reflective films. The organic reflective 296

film exhibits the highest average reflectivity of 95.7%. The aluminum foil shows a slightly lower average reflectivity of 91.0%, which can be attributed to SPR loss. In contrast, the Al-coated PET film demonstrates the lowest average reflectivity of 85.9%, resulting from the thinness of the aluminum coating.

In addition to reflectivity, the energy loss of X-rays within

the reflective films also significantly influences the over- 304

all output performance of the X-ray RL battery. Fig. presents the energy deposition profiles in the three types of reflective layers under irradiation from an X-ray tube operated at 50 kV. The aluminum foil exhibits the highest energy deposition, with 8.2% of the incident X-ray energy being absorbed within it. The Al-coated PET film shows a similar deposition profile to the aluminum foil within the first 1 corresponding to the aluminum layer, followed by a rapid decrease across the PET substrate. The total energy deposition in the Al-coated PET film is 1.0%, which is substan-

tially lower than that of the pure aluminum foil. The organic 315

reflective film maintains a low energy deposition throughout its entire thickness; however, due to its greater thickness of , the total energy deposition (1.7%) is slightly higher than that of Al-coated PET film. The output performance of the RL battery was evaluated both without any reflective layer and with each of the three types of reflective layers under X-ray irradiation at 50 kV and 1 mA tube current. The current density-voltage (J-V) characteristics for these four configurations are presented in Fig. (c). It is evident that the use

of any reflective film leads to a significant improvement in 325

performance compared to the control configuration without a reflector. Among the four configurations, the RL battery equipped with reflective film #3 demonstrates the highest performance. The corresponding output parameters are

summarized in Table. . The enhancement in battery performance is primarily attributed to an increase in short-circuit current density (J_{sc}). The values for batteries with reflective films #1, #2, and #3 are 15.3, 16.0, and 17.5 mA cm^{-2} , respectively, resulting in energy conversion efficiencies of 1.60%, 1.68%,

and 1.75%. The organic reflective film (#3), which combines 335

low X-ray absorption with the highest reflectivity, contributes to a 90% improvement in the energy conversion efficiency of the X-ray RL battery compared to the non-reflective configuration.

A quantitative analysis of the optical loss mechanisms in 340

the four battery configurations (without any reflective layer and with each of the three reflective films) was performed using Geant4 simulations. As illustrated in Fig. (d), the percentage of light coupled into the PV unit is 22.4% for the 344

control configuration, and 38.9%, 36.8%, and 41.0% for the

Sample FF(%) Control batteries with reflective films #1, #2, and #3, respectively.

The introduction of a reflective film effectively reduces optical loss at the top and side surfaces, thereby substantially enhancing the outcoupling efficiency. The degree of improvement

correlates with the reflectivity of the film. The organic reflective film (#3), which possesses the highest reflectivity, reduces top-surface

loss from 38.4% to 12.0%. In contrast, the Al-coated PET film (#2), with the lowest reflectivity, only reduces top-surface loss to 21.6%. However, the presence of the reflective film also prolongs the average light path within the scintillator, leading to a moderate increase in self-absorption

loss. For instance, when the organic reflective film is used, 357

self-absorption rises from 32.7% to 42.2%. In summary, the primary benefit of incorporating a reflective film lies in its ability to mitigate light escape from the top and sides, which

markedly improves optical coupling efficiency. The organic 361

reflective film, in particular, achieves an 83% improvement in outcoupling efficiency compared to the control configuration.

To assess the accuracy of the simulation results, the measured short-circuit current densities and the calculated incident light intensities were compared across the four battery configurations. Given that the external quantum efficiency

(EQE) of the PV units remains nearly constant across the light 368

intensity ranges studied in this work, the short-circuit current density can be considered proportional to the incident light intensity. Accordingly, both the

measured current densities and the simulated incident light intensities for all configurations were normalized to those of the control device and are presented in Fig. (e). The measured current densities for batteries equipped with reflective films #1, #2, and #3 are 159%, 167%, and 182% of the control device, respectively. corresponding calculated incident light intensities for these configurations are 158%, 162%, and 179% of the control, respectively. The slight discrepancies between the measured and calculated values are likely attributable to uncertainties in parameters such as the self-absorption coefficient. Both the incident light intensity and the current density are influenced by the outcoupling efficiency and the X-ray energy deposition rate. Although the Al-coated PET film (#2) has lower reflectivity than the aluminum foil (#1), its reduced X-ray absorption leads to a higher current density in the RL battery.

All configurations exhibit consistent trends between measurement and simulation, demonstrating the validity of the optimization strategy and the accuracy of the device model.

Optocoupler to enhance the light extraction The introduction of a reflective film effectively reduces optical losses from the top and side surfaces. However, it also elongates the average light path within the scintillator, leading to increased self-absorption losses. As depicted in Fig. an optical coupler adhesive (OA) layer was introduced between

the Cs 3 Cu 2 I 5 : Tl scintillator and the GaInP PV unit

to enhance light extraction from the scintillator and mitigate the extra self-absorption loss simultaneously. The OA layer reduces the intensity of total internal reflection and hence increased outcoupling efficiency of RL battery as a function of the refractive index of OA layer using the Geant4 model. It can be seen that the outcoupling efficiency increases with the increasing refractive index of OA layer when the refractive index is smaller than 1.8, the refractive index of scintillator (1.79). When the refractive index of OA layer is larger than 1.8, the total internal reflection at the interface

between the scintillator and PV unit disappears and the out-

coupling efficiency becomes constant. In this study, EGZ- SD65WH optical silicone grease, which has a refractive index of 1.46, was selected as the OA material to improve optical matching. The calculated outcoupling efficiency with silicone grease was 38.4%, representing a 67.7% increase compared to the battery without silicone grease.

As illustrated in the optical physical process in Fig. photons with large incident angles undergo total internal reflection (TIR) at the interface between the scintillator and the

PV unit. The introduction of an OA layer improves refrac-

tive index matching and enlarges the critical angle for light extraction from the scintillator. Fig. (c) displays the angular distribution of light emitted from

the scintillator with and without the OA layer. Without the OA layer, only photons with incident angles less than θ_c can escape the scintillator. The OA layer expands the escape angle from

θ_c to $\theta_{c'}$, thereby significantly improving the outcoupling

efficiency. Fig. (d) further compares the angular radiant intensity of the scintillator with and without the OA layer. The results exhibit a Lambertian emission profile, with peak intensity at (normal) and an intensity that drops off as the viewing angle increases. A noticeable increase in radiant intensity is observed across all angles. Fig. (e) presents the measured current density-voltage (J-V) characteristics of the RL battery with and without the OA layer under X-ray irradiation of an X-ray tube biased at 50 kV and 1 mA tube current.

The short current density of the device with the OA layer exhibits a substantial improvement (an increase of 65.6%), indicating the perfect alignment with the experimentally measured 67.7% improvement in outcoupling efficiency. These results convincingly demonstrate the efficacy of the OA layer in improving light extraction and overall performance of the RL battery.

- based X-ray RL battery with an optocoupler adhesive (OA) layer; (b) Calculated outcoupling efficiency of RL battery as a function of the refractive index of OA layer, marked with the silicone grease with a refractive index of 1.46; (c) Calculated angular distribution of lights exiting the scintillator with and without OA layer; (d) Calculated angular radiant intensity of scintillator with and without the optical coupling adhesive (OA) layer; (e) J-V curves of the RL battery with and without OA layer measured under the radiation of an X-ray tube biased at 50 kV and with a tube current of 1mA. (a) J-V curves of the RL battery with four battery configurations including (i) control (no addition layers), (ii) with a Organic reflection film (#3), (iii) with an optocoupler adhesive (OA) layer, and (iv) with both Organic reflection film and OA layers, measured under the radiation of an X-ray tube biased at 50 kV and with a tube current of 1mA; (b) Quantitative analysis of different optical loss mechanisms in the four battery configurations.

Sample FF(%) Control #3+OA uated the overall performance, as shown in Fig. (a). The cur- The performance of the RL battery incorporating both reflective film (#3) and an optical adhesive (OA) layer was eval-

rent density-voltage (J-V) curves demonstrate a further increase in current when both layers are applied. Detailed output parameters for all four configurations under 50 kV X-ray irradiation are listed in Table. . The battery equipped with both the #3 reflective film and the OA layer achieves a short-circuit current density (), a maximum output power density () of 12.9 , and an energy conversion efficiency of 2.15%, representing a 133.7% improvement over the control device. FFig. (b) presents a quan-

titative analysis of the optical loss mechanisms for the four 456

configurations, obtained from the Geant4 simulation. The incorporation of the OA layer substantially enhances light extraction from the bottom interface and reduces self-absorption

loss by shortening the internal optical path within the scintil- 460

lator. The combination of the reflective film and OA layer reduces the top-surface loss to 9.0% and the self-absorption loss to 36.2%, leading to the out-coupling efficiency of 51.0%, which is 222.2% of the control value and closely matches the experimental value of 221.8%. In summary, the key strategies for improving optical coupling efficiency in RL batteries

involve reducing the internal optical path length to minimize 467

self-absorption losses and suppressing light leakage at the top and side surfaces.

CONCLUSION

In summary, we have developed an effective method to improve the light collection efficiency in scintillator and suc-

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in RL batteries. The introduction of organic reflective lay- 476

ers and optical silicone grease as an optocoupler adhesive

successfully achieved a significant improvement in outcou- 478

pling efficiency of scintillator from 22.9% to 51.0%, resulting from the reduction of the self-absorption and surface leakage loss. Based on a scintillator and a spectrally

matched GaInP unit, the optimized RL battery demonstrated 482

an ultrahigh efficiency of 2.15% and an exceptional power density of 12.9 under the radiation of a tungsten- target X-ray tube at a 50kV tube voltage and 1.0mA tube current. Monte Carlo simulations confirmed the effectiveness of this strategy in suppressing self-absorption and light leakage losses, with theoretical analysis predicting a 222.2% improvement in optical coupling efficiency, which aligns closely with experimental results (221.8% improvement). These find-

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