Calibration and Correction Algorithm for the POLAR2/LPD Detector

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Abstract

Gas X-ray polarimetry refers to a class of detectors designed for measuring soft X-ray polarization. Systematic effects inherent to these detectors introduce residual modulation, resulting in systematic bias in the detected polarization of sources. This work discusses these systematic effects and their calibration and correction in the Gas Micro-channel Pixel Detector (GMPD) prototype for Polar2/Low-energy X-ray Polarimetry Detector (LPD). Furthermore, we propose an algorithm that integrates parameterization with Monte Carlo simulation and Bayesian iteration to eliminate residual modulation. Following data correction, the residual modulation at various energy points has been reduced to below 1%, and a good linear relationship between the degree of polarization and modulation factor is observed. The improvement in modulation factor after correction ranges from 2% to 15%, surpassing the performance of IXPE above 5 keV.

Full Text

Preamble

Calibration and Correction Algorithms for the POLAR2/LPD Detector

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Gaseous X-ray polarimetry refers to a class of detectors used for measuring the polarization of soft X-rays. The systematic effects inherent in such detectors introduce residual modulation, leading to systematic biases in the polarization detection results of the source. This paper discusses the systematic effects and their calibration and correction using the Gas Microchannel Plate–Pixel Detector (GMPD) prototype for Polar2/Low Energy X-ray Polarization Detector (LPD). Additionally, we propose an algorithm that combines parameterization with Monte Carlo simulation and Bayesian iteration to eliminate residual modulation. The residual modulation after data correction at different energy points has been reduced to below 1%, and a good linear relationship is observed between the polarization degree and modulation degree. The improvement in modulation degree after correction ranges from 2% to 15%, and the results exceed those of IXPE above 5 keV.

Keywords: Gaseous X-ray polarimetry, Residual modulation, Bayesian approach

Introduction

In recent decades, there has been a growing interest in the field of gamma-ray astronomy, particularly in the study of Gamma-ray bursts (GRBs) [?], which are highly energetic cosmic events. While satellite observations from missions like Swift [?] and Fermi [?] have yielded valuable insights into the energy spectra and timing properties of GRBs, numerous fundamental questions remain unanswered. These include understanding the mechanisms that propel the energetic jets, elucidating the processes responsible for energy dissipation, determining the composition of the jets, investigating the configurations of magnetic fields, and unraveling the mechanisms behind particle acceleration and radiation [?]. The detection of polarization in GRBs plays a crucial role in providing important clues for addressing the aforementioned issues [?].

Scheduled for deployment in 2026 as an external payload on the China Space Station, POLAR-2 [?] is the successor experiment to POLAR [?]. Its main goal is to conduct high-precision measurements of polarization across the spectrum from soft X-rays to gamma rays. The GMPD [?] is an innovative gas pixel detector developed to validate the design of the POLAR2/LPD [?] payload. Recently launched IXPE [?], PolarLight [?], and the under-development eXTP [?] and Polar-2/LPD all utilize gas pixel polarimetric detector structures. This type of detector has high spatial resolution, capable of imaging electron tracks at the level of hundreds of micrometers, thus providing excellent sensitivity in polarimetric detection. However, due to the complex and sophisticated structure of the gas pixel detector, as well as its high spatial resolution sensitivity, the operational state of the instrument, various components, and electronic devices may introduce systematic effects on the polarimetric detection results. These systematic effects can result in non-zero modulation named residual modulation when detecting unpolarized sources, leading to systematic biases in the measurement of polarized sources. Since low-energy electron tracks are relatively short,

the residual modulation effects produced by these systematic effects are more significant in low-energy events and cannot be ignored.

For residual modulation, IXPE employs two methods for correction [**?**]: the first involves oscillating the detector during the detection process to integrate and eliminate some of the systematic effects. The second method involves calibrating the corresponding Stokes parameters q and u for systematic effects in different regions and energy points, and then subtracting them on an event-by-event basis to eliminate the systematic effects. In this research, we listed some of the known causes of residual modulation and corrected some of these effects based on their generation mechanisms. For another part of the residual modulation where the specific causes are currently unclear, we proposed a correction algorithm and obtained favorable outcomes.

In this paper, we first introduced the basic structure and polarization detection principles of the Polar2/LPD detector in Sect. II. We then discussed the residual modulation caused by signal response and its correction methods in Sect. III. In Sect. IV, we discussed the residual modulation caused by geometric effects and proposed a modulation curve correction method based on the parameterization of scale ratios, combined with Monte Carlo simulation and Bayesian iteration [**?**] (see in Appendix A), and provided the errors of this algorithm. Subsequently, we compared various data reconstruction characteristics before and after algorithm correction and compared them with the modulation calibrated by the IXPE detector. Finally, in Sect. V, we discussed the performance of the GMPD after correction, emphasizing the performance and scalability of the correction algorithm, and outlined prospects for future work.

II. Geometric Structure and Working Principle of LPD

The LPD system shown in Fig. 1 is composed of a total of 9 detector modules, arranged in a 3×3 array configuration. Each detector module consists of 9 detection units with 90° field of view (FoV), resulting in a total of 81 detection units. A detection unit of LPD consists of working gas, a Gas Micro-Channel Plate (GMCP) [**?**], a pixel readout chip, and frame structure. Working gas serves the purpose of photoelectric effects and formation of ionization tracks. The upper end of the gas chamber is sealed with a 50 μm beryllium window, which prevents entry of lower energy photons and ensures gas containment to prevent leakage. The GMCP layer is positioned near the bottom plane of the chamber, for the purpose of electron avalanche multiplication. At the bottom of the chamber is the chip. The intended chip version, Topmetal-L, which is expected to be formally integrated into LPD, will undergo optimization in terms of power consumption, effective area, and resolution based on the existing chip version, Topmetal-II [**?**].

The soft X-rays, as shown in Fig. 2, pass through the beryllium window of the detector unit and have a certain probability of undergoing photoelectric effects within the drift region, resulting in the generation of photoelectrons. These

photoelectrons carry the polarization information of the incident photons. Photoelectrons deposit ionization energy within the gas and generate secondary ionization electrons until they come to a complete stop. Within the induction region, an upward-directed electric field is applied, causing some of the secondary ionization electrons to drift downward onto the surface of the GMCP. A portion of these electrons enters the micro-channels and undergoes avalanche multiplication. The multiplied electrons then emerge from the lower surface of the GMCP, where some of them are absorbed, resulting in the production of a pulse signal. The remaining multiplied electrons continue to drift towards the Topmetal chip, inducing signals in the corresponding pixel positions. This process allows the projection of the photoelectron track onto the 2D plane of the Topmetal chip, enabling us to obtain the projection results.

In general, the angular distribution of photoelectrons detected by the gas pixel detector is modulated by polarized X-rays. For gas pixel detectors, photons primarily interact with the K-shell electrons of gas molecules through photoelectric interactions, and the direction of electron emission is described by the differential cross-section according to the following formula [**?**]:

$$\frac{d\sigma}{d\Omega} \propto \frac{\sin^2\theta \cos^2\phi}{(1 + \beta\cos\theta)^2}$$

where β is the emission velocity of the photoelectron in units of the speed of light c, θ and ϕ are the latitude and azimuth angles, respectively. Due to the lack of resolution in the Z direction for the LPD detector, we reconstruct the 2D projection angular distribution of the azimuthal angle of the photoelectron emission, corresponding to the integration of θ in the formula. Therefore, the reconstructed angular distribution is modulated by the $\cos^2$ factor. In theory, for 100% polarized X-rays, the minimum value of the true emission distribution in ϕ should be 0. However, due to limitations in instrument resolution, system effects, and reconstruction algorithm accuracy, there will be a certain proportion of unmodulated components in the angular distribution, as shown in Fig. 3 (a), (b). Therefore, the modulation function of ϕ, $M(\phi)$ can be written as:

$$M(\phi) = A + B\cos(2(\phi - \phi_0))$$

Therefore, the modulation factor μ is defined as the ratio of the area occupied by the modulation component in the distribution:

$$\mu = \frac{B}{2A + B}$$

III. Calibration and Correction of Signal Response

The structural design and operational principles of GMPD result in variations in the response between pixels, which can impact the energy resolution of the

detector. More importantly, some of these factors can introduce anisotropic differences, leading to residual modulation. This section primarily discusses the impact and calibration of these factors.

A. Pixel response differences

Due to the subtle structural differences between each pixel, the uniformity of the electric field, and the uniformity of GMCP gain, the signal induction intensity of drift charge varies among different pixels. It is necessary to calibrate the relative signal induction intensity on each pixel. We uniformly irradiate with a 4.51 keV flat source and statistically record the signal distribution received by each pixel. As the response curve of the pixels exhibits good linearity [**?**], we can characterize the relative signal induction intensity of a pixel by the mean of the signal distribution received on that pixel. In the process of calculating the mean, we only selected the part of the signal intensity greater than 50 in order to eliminate the interference of noise. Fig. 4 illustrates the average distribution of pixel ADC values before and after correction.

B. Rolling-Shutter and Signal Decay

Another source of residual modulation is the attenuation of pixel signal amplitude caused by signal readout time delay. Since Topmetal-II adopts a rolling-shutter readout method to read each frame of the image, pixel signals are read out in sequence, which means there is a certain delay from the triggering of the induction signal to the readout, and there is also a delay in the readout time of different pixels on the same track. The individual pixel CSA structure of Topmetal-II is shown in Fig. 5(a), where the pixel controls the discharge of induced charge through the drain voltage. Therefore, the scanned readout signal will be attenuated compared to the true signal amplitude at the triggering moment due to the time delay. The scanning time for one frame of Topmetal-II is $\tau_{\mathrm{frame}} = 2.59$ ms, and the scanning time interval for each pixel is $\tau_{\mathrm{pixel}} = 500$ ns. Due to the rolling-shutter method of scanning the chip column by column along the 0° direction, the scanning time interval between adjacent pixels in the 90° direction is 35 μs, while the scanning time interval between adjacent pixels in the 0° direction is 500 ns, with $\Delta T_{0°} \ll \Delta T_{90°}$. The difference in scanning time intervals between 0° and 90° can result in inconsistent signal attenuation gradients in these two directions, introducing a vertical bias, namely, residual modulation in the 90° direction.

In order to calibrate the systematic errors caused during the scanning process, it is first necessary to calibrate the signal attenuation behavior of each pixel, and secondly to determine the time difference between each triggered and readout pixel. We input square wave signals to the chip and record the output results of the pixel readout signals for multiple consecutive frames, in order to obtain the decay characteristics of each pixel and perform parameter fitting. The theoretical formula for pixel decay is given by Equation 4:

$$A(t) = a \cdot \exp\left(-\frac{t - t_0}{b \cdot (t - t_0) + c}\right)$$

Fig. 5(b) illustrates the decay pattern of signal intensity over time on a pixel and the fitting result. Fig. 5(c) shows the decay time distribution of all pixels on Topmetal-II, indicating that the typical decay time scale for pixels is 20 ms.

The time precision of GMCP is 10 ns [**?**]. The time difference Δt is obtained by comparing the trigger signal of GMCP and the trigger signal position on Topmetal-II. Since the typical time scale required for electron propagation in GMPD is on the order of tens of ns, it can be neglected compared to the characteristic time scale of pixel decay. Based on the time difference, we can then correct the decay signal for each pixel using the following formulas:

$$A_{\text{truth}} = a \cdot \exp\left(-\frac{t_0 - \Delta t}{b \cdot (t_0 - \Delta t) + c}\right)$$

C. Charge pile up effect

The encapsulated detector exhibits an initial stage where the gain increases with the accumulated number of events, as illustrated in Fig. 6(a). This effect is attributed to charge accumulation. The surface of the Topmetal-II utilized in the detector features a grid-like insulating layer, causing electrons that fall and become adsorbed on this layer to have limited mobility. As the accumulation of avalanche multiplied electrons rises, the potential on the chip surface gradually alters, impacting the charge collection efficiency and modifying the gain, as depicted in Fig. 6(b).

If the charge accumulation process is unevenly distributed on the surface of the chip, it will lead to a noticeable signal intensity gradient on the chip surface, eventually resulting in the generation of pseudo-modulation perpendicular to the gradient direction. Fig. 7 illustrates the residual modulation caused by the charge accumulation effect. Initially, a ferrous strip was used to partially obstruct a section of the detector's field of view, leaving a gap of a few millimeters. Following a 2-hour exposure to an X-ray flat source, the obstruction was removed, and a 5.9 keV unpolarized Fe55 source was used to irradiate and collect the photoelectron tracks. Upon reconstruction, it was observed in Fig. 7(a) that the signal gain at the previous narrow gap position was significantly higher than the shaded area, and the residual modulation in the narrow gap area was higher than in the shaded area, with the modulation direction parallel to the gap. Subsequently, without any obstruction, the X-ray flat source was used again for 4 hours to accumulate charges on the entire surface of the chip to near saturation. The detector was then irradiated with the 5.9 keV unpolarized Fe55, and the tracks were reconstructed in Fig. 7(b). Comparing the results of the Fe55 measurements before and after charge accumulation reached saturation, it was found that the residual modulation caused by the uneven gain due

to charge accumulation significantly decreased. Therefore, it is possible to mitigate the impact of the charge accumulation effect by calibrating or measuring the detector after saturating the charge accumulation before conducting experiments. Since the accumulated charge is unlikely to naturally dissipate, once the detector is encapsulated, only one thorough charge accumulation is required.

By employing Garfield++ and COMSOL for charge drift accumulation iteration and updating of the drift electric field, we successfully replicated this effect in simulations, as indicated by the blue data points in Fig. 6(a), which align with the experimentally observed gain variation results. The process of charge accumulation can be described by a simplified Eq. 7:

$$\frac{dq}{dn} = a_c \cdot (q_{max} - q)$$

Where n is the number of events, q is the accumulated charge on the chip, q_{max} is the maximum saturated accumulated charge, and a_c is the charge adsorption coefficient. Therefore, the change in the accumulated charge quantity with respect to the detector counts, $q(n)$, can be expressed in a parametric form as given in Eq. 8:

$$q(n) = x_0 + x_1 \exp(x_2(n + x_3))$$

Both experimental and simulation results indicate that the charge accumulation process gradually reaches saturation, leading to a stable final gain. Additionally, the non-focusing observation mode of the LPD can prevent the uneven accumulation of charge on the chip surface. Therefore, after a sufficient number of accumulated events, the impact of the pseudo-modulation caused by the charge accumulation effect in the encapsulated detection unit can be reduced to a negligible level.

IV. Calibration and Correction of Geometrical Effects

A. Pixelization influence

As shown in Fig. 8(a), we consider a shorter track with a circular projection. Due to the parallel arrangement of Topmetal-II chips in the X and Y directions, the signal distribution sensed on the chip pixels exhibits anisotropy for such tracks. The symmetry is most pronounced in the directions of 0° and 90°, which are aligned with the pixel arrangement. The commonly used moment analysis algorithm for such shorter tracks calculates the centroid line of the pixel track to determine the direction of electron emission. This can lead to a bias in the reconstruction direction of these tracks towards 0° and 90°.

To mitigate the residual modulation caused by pixel arrangement, we need to exclude events with too few responsive pixels and events that are too short or too circular during event selection. Therefore, during reconstruction, we only

select events with a number of hit pixels greater than or equal to 27 and exclude the bottom 20% of events with smaller ellipticities. Fig. 8(b) below shows the angular distribution of the reconstructed unbiased events before and after the event selection. After the event selection, the residual modulation caused by pixel arrangement is significantly improved.

B. Truncation effect

Similarly, due to the Rolling-Shutter line-by-line scanning readout of the chip, if an event occurs precisely at the position covered by the pixels being scanned at that moment, the event will be truncated and appear in both the preceding and subsequent frames. If the truncated part in one frame has fewer fired pixels that do not exceed the threshold, we can only obtain an incomplete truncated event. As the edge of the truncated track is always parallel to the scanning direction, it introduces a systematic bias in scan direction.

Thus, we continue to utilize the time information from GMCP and Topmetal-II to determine if an instance is truncated. Considering the combined time resolution of GMCP and Topmetal-II is 262 ns [**?**] and τ_{pixel}, we determine if a track is truncated by examining whether the pixel scanned when the signal arrives and the positions of the five pixels before and after it precisely overlap with the region covered by the photoelectron track signal.

C. Track image distortion

Excluding the systematic effects and corrections discussed above, the angular reconstruction of track data obtained from the detector still exhibits some residual modulation. This may partly be attributed to the geometry and potential distribution of the detector. The gas cavity of the LPD detection unit is not completely symmetrical. As shown in Fig. 9, in addition to the charge induction chip Topmetal, a temperature and pressure sensor chip is also placed nearby. This placement leads to a relatively significant distortion of the electric field near the side of the Topmetal chip adjacent to the sensor chip, resulting in a noticeably higher residual modulation on that side.

Furthermore, there is a 1 mm wide and 0.8 mm deep groove between the charge induction collection plane of the Topmetal chip and the base plane of the detection unit. Additionally, several to a dozen bonding wires are present around the chip. The geometric structure of the chip's edge and the potential on the bonding wires also cause distortion of the electric field at the edge of the chip. Consequently, it can be observed that the direction of the residual modulation reconstructed in the edge portion of Fig. 7 is generally perpendicular to the edge of the chip. Therefore, in order to minimize the influence of edge electric field distortion on the reconstruction, we choose to exclude events within 12 pixels of the charge center distance from the edge when selecting valid events.

The residual modulation distribution in different regions near the center of the chip appears to be more random. This variability in residual modulation in

certain regions may stem from systematic process issues during chip etching, subtle irregularities during detector installation, and the uneven accumulation of charge resulting in differences in the electric field across different areas of the chip. These issues can all impact the electric field distribution near the chip surface, and the distortion of the electric field can alter the track shape. This alteration is often nonlinear, and the impact on tracks at different positions, heights, and lengths varies. As a result, we lack sufficiently precise information to make pixel-by-pixel or event-by-event corrections from a first-principles perspective for the obtained tracks in the experiment.

The deformation of tracks is reflected in the differences in position resolution in different directions of the detector. As shown in Fig. 10, at different energy points, the position resolution in the X direction of the detector is worse than that in the Y direction. This indicates that the distortion of the track is more severe in the X direction, and this anisotropic deformation of tracks leads to excessive stretching in the X direction, resulting in significant residual modulation.

Similar residual modulation issues also arise in the IXPE detector. The correction scheme for residual modulation provided by IXPE involves calibrating experimental scales for each chip region to correct the Stokes parameters required for event reconstruction. Since the IXPE detector needs to image the observed objects, segmenting and correcting different regions is necessary. However, for the LPD, which lacks imaging capabilities, photons from the source will uniformly fall on the entire chip surface. Therefore, the LPD only needs to consider correcting the distribution of residual modulation integrated over the entire chip surface for events. To address this, we propose a Bayesian method combined with Monte Carlo simulations to correct residual modulation.

1. Correction algorithm

When correcting the data for an energy point, we only need to calibrate a correction parameter $\bar{\eta}$: the ratio of the pixel size in the Y direction to the pixel size in the X direction. We can phenomenologically explain the need to introduce the parameter $\bar{\eta}$: the distortion of the electric field will cause the equipotential surfaces to no longer be parallel to the Topmetal chip plane. Therefore, by projecting the chip plane onto the deformed equipotential surface, the linearity in different directions of the chip will have different scaling rates. We select the ratio of the scaling rates calibrated in the two directions parallel and perpendicular to the scanning direction as $\bar{\eta}$. It should be noted that the $\bar{\eta}$ value for different regions of the chip is different. However, because the LPD does not have polarized imaging capabilities, the correction parameter we consider is actually the weighted average value $\bar{\eta}$ of the parameters for different chip regions.

Calibrating $\bar{\eta}$ requires a comparison of experimental data and simulations. Taking the 5.40 keV energy point as an example, we calibrated the modulation

curves obtained from a 99.9% polarized source at 0°, 30°, 60°, 90°, 120°, and 150° polarization phases. It can be observed that due to residual modulation, there are significant differences in the modulation at these phases, with a difference of approximately 18% between the modulation at 0° and 90° as shown in Fig. 15(g).

Since residual modulation is an inherent property of the detector and is independent of the polarization phase of the source, the overall modulation curve measured is a result of the superposition of residual modulation and source modulation. Therefore, the overall modulation curve can be described as:

$$M_{\mathrm{Obs}}(\phi) = M_{\mathrm{Res}}(\phi) \cdot M_{\mathrm{Source}}(\phi, \phi_0)$$

Where M_{Obs} is the modulation curve obtained from reconstructed angular distribution data, M_{Res} represents the impact of residual modulation, and M_{Source} is the modulation curve generated by the polarized source. At normal incidence, the form of M_{Source} is:

$$M_{\mathrm{Source}}(\phi, \phi_0) = A\cos(\phi - \phi_0)^2 + B$$

According to equation 10, we observe that M_{Source} is modulated by $\cos^2$. Therefore, by equally combining two sets of data with a 90° difference in polarization phase, the modulation caused by the polarized source can be eliminated. As a result, when equally mixing six sets of data at 0°, 30°, 60°, 90°, 120°, and 150° polarization phases, the modulation curve of the angular distribution $M_{\mathrm{Obs}} \propto M_{\mathrm{Res}}$. The modulation distribution of the combined data is shown in Fig. 11. The combined results indicate that the residual modulation distribution still follows equation 10, and fitting different combined data sets within the error range shows that the residual modulation values obtained from different data sets are consistent, with the phase of the residual modulation being 0°.

We obtained the residual modulation amplitude at the 5.40 keV energy point by fitting the residual modulation curve from Fig. 11(d). Next, we consider using simulations to reproduce the same residual modulation distribution and obtain a response matrix for correcting the residual modulation in the experimental data. We utilized the star-XP software framework [**?**] specifically designed for the LPD detector. The simulation framework meticulously simulates the interaction processes between photoelectrons and the detector, as well as the digitization process. The simulated data output by the framework shows good agreement with the experimental data. Our operational procedure followed the steps below:

1. In the simulation framework, we simulated the tracks of 1.5 million unpolarized 5.40 keV X-ray photons and maintained the parameters set in the simulator consistent with the actual operating parameters of the detector.

2. Initially, we set $\bar{\eta} = 1$, representing the state of the detector without electric field distortion, and simulated the two-dimensional image of the photo-

electron tracks after digitization. We reconstructed each of the 1,500,000 tracks without distortion to obtain the reconstructed angle information, $\text{Angle}_{\text{Truth}}$. It is important to note that this is not the true value of the emission angle of the photoelectrons provided by the simulation, but rather the angle value obtained from the reconstruction. The distribution of $\text{Angle}_{\text{Truth}}$ is shown in Fig. 12(a).

3. In the simulation, we adjusted the value of $\bar{\eta}$ to deviate from 1, representing the occurrence of electric field distortion in the detector. We used the photoelectron track simulations from Step 1 after digitization, and due to different scaling in the X and Y directions, the reconstructed angle distribution, $\text{Angle}_{\text{Distor}}$, exhibited a non-zero residual modulation. When $\bar{\eta} < 1$, the phase of the residual modulation is 0°, consistent with the experimental data. By adjusting the value of $\bar{\eta}$, we were able to align the modulation amplitude of the $\text{Angle}_{\text{Distor}}$ distribution with Fig. 11(d), as shown in Fig. 12(b). For 5.40 keV, the value of $\bar{\eta}$ was determined to be 0.981.

4. Combining the $\text{Angle}_{\text{Truth}}$ and $\text{Angle}_{\text{Distor}}$ reconstructed step by step in the second and third steps, we can obtain the response matrix M_{Distor}, which arises due to the adjustment of the parameter $\bar{\eta}$. The physical interpretation of M_{Distor} is as follows: if we denote N_{Truth} as the number of instances for which the reconstructed angle falls within the i-th bin when $\bar{\eta} = 1$, then the number of instances for the same events after adjusting $\bar{\eta}$ and reconstructed within the j-th bin is given by equation 11:

$$N_{\text{Distor}} = \sum_i N_{\text{Truth}} \cdot M_{ij}$$

In other words, the element (m, n) of M_{Distor} is proportional to the probability value $P(n|m)$: the probability that an event originally reconstructed in the m-th bin is reconstructed in the n-th bin due to the adjustment of $\bar{\eta}$.

After obtaining the parameter $\bar{\eta} = 1$ that describes the system effect and its corresponding response matrix M_{Distor}, we employed a Bayesian iterative process algorithm to decouple the modulation distribution generated by the polarization source, which does not have electric field distortion, from the overall system effects. Many software packages offer Bayesian algorithm capabilities, and in our study, we utilized the RooUnfoldBayes packages integrated within RooUnfold [**?**]. The RooUnfoldBayes package is capable of iteratively restoring the input angular modulation distribution to its undistorted state, based on the provided response matrix M_{Distor}, and automatically calculates the errors for each bin following the Bayesian iteration process.

The use of Bayesian methods involves the selection of prior distributions and the adjustment of the number of iterations. Firstly, due to the periodicity of the modulation curves with a period of π, monotonically increasing or decreasing

distributions are not appropriate. Therefore, for simplicity, we set the prior distributions to uniform distributions. Secondly, concerning the number of iterations, we determine the convergence of the iteration process by comparing the χ^2 values of the distributions $M(\phi)_{n+1}$ and $M(\phi)_n$ after the $n+1$-th and n-th iterations. We found that when the number of iterations is set to 10, the χ^2 values for different phases, polarizations, and energies are all less than 0.5, which indicates that the iterative process has essentially reached convergence. Additionally, after 10 iterations, the introduced iteration errors in each bin are relatively small. Therefore, we set the number of iterations to 10. Fig. 13(a) illustrates the variation of the χ^2 values corresponding to different numbers of iterations, while Figs. 13(b) and 13(c) present the corrected results for the 5.40 keV 99.9% polarized data at 0° and 90° phases, respectively.

2. Result

At a specific energy point, using the aforementioned method, we only need to calibrate one corresponding parameter, namely $\bar{\eta}$, and simulate the response matrix at that energy point. This allows for the application of Bayesian iteration to correct the modulation curves at different polarization degrees and phases. The corrected polarization degree and modulation level exhibit a good linear relationship, and the modulation levels at different phases also show good consistency. Fig. 14 illustrates the comparison of the modulation distribution before and after correction for experimental data at 5.40 keV and 90° polarization phase, ranging from unpolarized to 99.9% polarized. When the polarization degree is low, the residual modulation will dominate the distribution of the modulation curve. At this point, the unrevised experimental data reconstruction results will exhibit significant deviations. In contrast, the corrected data maintains good stability in the reconstruction of the polarization phase, while also exhibiting a strong linear relationship between the modulation level and the polarization degree. Fig. 15 displays the comparison of experimental data before and after correction at several energy points, including 2.98 keV, 4.51 keV, 5.40 keV, 6.40 keV, and 8.05 keV, for different polarization phases and degrees. The uncorrected data, due to the residual modulation not being eliminated, exhibit significant differences in the reconstructed modulation degree at different phases. For example, at 4.51 keV, the modulation degrees at 0° and 90° for the same fully polarized source differ by approximately 18%. The polarization phase reconstruction results from the uncorrected data also show a significant deviation from the true values, especially in the direction that differs by 90° from the polarization direction of the residual modulation. However, after Bayesian iterative correction, the polarization data show good consistency in modulation degree across different phases. Additionally, the polarization degree and modulation degree exhibit a good proportional relationship, meeting the calibration requirements of the LPD.

3. Error and Comparison

The error in the modulation degree of the corrected data distribution mainly arises from two sources. One part originates from the statistical error of the data, which can be obtained through fitting. The other part of the error arises from the process of using the Bayesian method for correction:

1. Error propagation in the Bayesian iteration process: This error can be calculated through the error propagation matrix A_4.

2. Termination of the Bayesian iteration: Although the chi-square calculation results show good convergence after 10 iterations for all experimental data, the convergence levels of the data at different polarization phases are inconsistent due to the fixed number of iterations. This results in slight differences in the reconstructed modulation degree at different polarization phases after correction.

3. Parameterized response matrix: The error in the estimation of the parameter $\bar{\eta}$ provided by the simulator will be propagated to the response matrix, and during the Bayesian iteration process using the response matrix, the error will be propagated to the corrected data's modulation degree.

The error propagation in point 1 is calculated by the RooUnfold package. For the statistical error of the data and points 1 and 2, due to the dependence of the Bayesian method iteration process on the original data itself, it is difficult to decouple and analyze the contributions of these two parts. Therefore, a unified error estimation is provided using the modified Bootstrap method, and this part of the error is denoted as σ_{unfold}: Sampling 10,000 times at a certain polarization degree (taking fully polarized data as an example).

1. Each sampling involves 100,000 with-replacement samplings of the data at 0°, 30°, 60°, 90°, 120°, and 150° phases in the experiment.

2. Reconstruction of the sampled data at the six phases is performed, and the Bayesian method is used to correct the reconstructed angular distribution results. Six sets of corrected data are fitted to obtain six modulation degrees.

3. Random weights are assigned to the six modulation degrees, with the total sum of the six weights equaling 1. The weighted sum yields the modulation degree for this sampling.

After 10,000 samplings, a distribution of the modulation degrees is plotted, and a Gaussian fit is applied. The fitted sigma represents the σ_{unfold}. Fig. 17 illustrates the modulation distribution of several energy points sampled using the modified Bootstrap method from completely polarized data, and the σ_{unfold} obtained from Gaussian fitting.

For point 3, the error introduced by parameterization can be propagated to the error of the response matrix by providing the error of the parameter $\bar{\eta}$. This

error is ultimately propagated to the error of the modulation degree. The error introduced by parameterization is denoted as σ_{para}. We obtain the error of $\bar{\eta}$ as follows: by making a slight adjustment to the value of $\bar{\eta}$ corresponding to a specific energy point, denoted as $\Delta\bar{\eta}$. After the adjustment, we incorporate the parameter $\bar{\eta} + \Delta\bar{\eta}$ into the Star-XP simulation software to simulate 1,500,000 events, and reconstruct their angular distributions. When the χ^2/ndf between this adjusted angular distribution and the angular distribution obtained from the simulation with $\bar{\eta}$ equals 1, the $\Delta\bar{\eta}$ represents our estimated error of $\bar{\eta}$. We apply the modified Bootstrap method to resample the data 10,000 times using the response matrix obtained from the parameter value $\bar{\eta} \pm \Delta\bar{\eta}$, and then perform Gaussian fitting to obtain the total error $\sigma_{\mathrm{unfold+para}}$ or denoted as σ_{sys}. The contributions of the various error terms at different energy points and the modulations corrected are presented in Table 1.

Furthermore, we compared the variation trends of $\bar{\eta}$ and the ratio of position resolution in the Y and X directions of the detector at different energies, as shown in Figure 11, the trends are in good agreement. Fig. 18(a) demonstrates the modulations at several energy points before [?] and after Bayesian correction, and compares them with the calibration results of the IXPE detector [?]. Comparing the modulations before and after correction, the modulations after correction are higher at each energy point than before correction. Comparing the corrected modulations with the results from IXPE, when the energy is below 4.51 keV, our detector's modulations are lower than the IXPE calibration results. The charge induction chip pixel size of IXPE (60 μm) is smaller than the pixel size of our current Topmetal-II (83 μm), resulting in shorter reconstructed tracks for low-energy photons and higher reconstruction accuracy requirements for resolution. Therefore, the modulation of the reconstructed tracks for the low-energy part is lower than the IXPE results. However, when the energy is higher than 4.51 keV, the corrected modulations are higher than the IXPE results, possibly due to the better signal-to-noise ratio of Topmetal-II. For longer tracks, the pixel resolution no longer plays a decisive role in reconstruction accuracy, and factors such as chip noise, the diffusion coefficient of secondary ionization electrons, detector gain, track length, and others begin to have a greater impact on the reconstruction. More importantly, after correction, the residual modulations of the detector at several energy points have been reduced to levels below 1%. In addition, the residual modulation result at 5.9 keV in Fig. 18(b) is obtained using the $\bar{\eta}$ at 5.4 keV. The result of the response matrix correction at 5.9 keV is $0.24\% \pm 0.59\%$. The energy resolution at 5.4 keV, corresponding to the detector, is approximately 19.5% [?], and 5.9 keV coincides with the boundary value of the 5.4 keV energy resolution. This result indicates that the calibration parameter $\bar{\eta}$ can be extended to the energy resolution range of the detector at several energy points, while still maintaining good correction results.

V. Summary and Outlook

This paper discusses the systematic effects of GMPD and corrects the residual modulation of modulation curves caused by various systematic effects. GMCP is a prototype detector designed for Polar-2/LPD, and the study of GMPD systematic effects is of great significance for the subsequent design and performance optimization of LPD, reducing systematic effects, and calibrating detector polarization performance. In the second section, we list several main systematic effects that lead to residual modulation, including differences in gain and layout of chip pixels, signal attenuation in electronics, track truncation, and charge accumulation effects. For these known systematic effects, we corrected them through calibration, setting threshold conditions, and time positioning. For the remaining residual modulation caused by a part of the systematic effects, we obtained the response matrix through parameterization combined with Monte Carlo simulation and used the Bayesian method to eliminate the contribution of residual modulation in the modulation curve. The final results show that the residual modulation of the data corrected by our algorithm has been reduced to below 1% at various calibration energy points. The reconstructed modulation degrees of data at different polarization phases show good consistency, and the polarization degree and modulation degree also exhibit a good linear relationship. At the same time, we discussed the errors of the correction algorithm proposed in this paper and compared the corrected modulation results with the IXPE calibration results. The data results of GMPD after correction by our algorithm show higher polarization detection performance than IXPE above 5 keV.

The results of this paper indicate that the correction algorithm proposed by us can be well applied to the correction of systematic effects in the LPD detector. Additionally, our parameterized correction algorithm can naturally be extended to the study and correction of oblique incidence systematic effects. The correction algorithm that introduces Stokes parameters in IXPE is established under the condition of normal incidence. When photons are obliquely incident, the description of photoelectrons using the Stokes parameter system is incomplete [**?**], making it difficult to extend to the correction of oblique incidence systematic errors. The large field-of-view design of LPD implies that most of the time we need to analyze obliquely incident data results. Based on the method proposed in this paper, we will also carry out the reconstruction and study of oblique incidence systematic effects in the future.

Appendix A: Bayesian iterative method

The Bayesian iterative method is a statistical technique used to estimate a probability distribution by iteratively updating prior beliefs with new evidence. It is employed to correct for detector effects and estimate the true distribution of a physical variable from the measured data.

In Bayes method, the unfolded distribution, $\hat{n}(C_i)$, is given by applying the

unfolding matrix M_{ij} to the measured distribution, $\hat{n}(E_j)$, as shown in the following equation A1:

$$\hat{n}(C_i) = \sum_{j=1}^{n_E} M_{ij} n(E_j)$$

The unfolding matrix is given by:

$$M_{ij} = \frac{P(E_j|C_i)n_0(C_i)}{\sum_{k=1}^{n_C} P(E_j|C_k)n_0(C_k)} \cdot \frac{1}{\epsilon_i}$$

$P(E_j|C_k)$ is the element of response matrix R. ϵ is defined as $\epsilon_i \equiv \sum_{j=1}^{n_E} P(E_j|C_i)$. In the first round of Bayesian iteration, $n_0(C)$ is set based on prior knowledge, while in subsequent iterations, $n_0(C)$ will be replaced by the $\hat{n}(C)$ obtained from equation A1. $\hat{n}(C)$ will be updated with each iteration.

The computation of the error propagation matrix in the Bayesian method is given by the following equations A3-A4:

$$\frac{\partial \hat{n}(C_i)}{\partial n(E_j)} = M_{ij} + \sum_{k=1}^{n_E} M_{ik} n(E_k) \left(\frac{1}{n_0(C_i)} \frac{\partial n_0(C_i)}{\partial n(E_j)} - \frac{\sum_{l=1}^{n_C} n_0(Cl)\frac{\partial n_0(Cl)}{\partial n(E_j)}}{\sum_{l=1}^{n_C} n_0(Cl)} \right)$$

$$V(\hat{n}(C_k), \hat{n}(C_l)) = \sum_{i,j=1}^{n_E} \frac{\partial \hat{n}(C_k)}{\partial n(E_i)} V(n(E_i), n(E_j)) \frac{\partial \hat{n}(C_l)}{\partial n(E_j)}$$

Here, $V(n(E_i), n(E_j))$ is computed from the measurement data.

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