

## Postprint: Experimental Study and Energy Analysis of CO<sub>2</sub> Thermosyphons for Data Center Free Cooling

**Authors:** Zhang Hainan, Shao Shuangquan, Tian Changqing, Jin Tingxiang

**Date:** 2017-11-07T00:00:00+00:00

### Abstract

Natural cooling technology for data center rooms is gaining increasing attention as an effective energy-saving cooling method for data centers. Natural cooling devices based on thermosyphons exhibit excellent heat transfer performance under small temperature differences and possess promising application prospects. This paper presents experimental and energy-saving effect analysis studies on thermosyphons for data center natural cooling using CO<sub>2</sub> as the working fluid, with comparisons made to R22. Experimental results demonstrate that, compared to R22 as the working fluid, the performance of CO<sub>2</sub> thermosyphons is more significantly influenced by the filling ratio. The optimal filling ratio is 150%, which is higher than that of R22. Under optimal filling ratio conditions, the heat transfer capacity of both CO<sub>2</sub> and R22 thermosyphons increases with increasing indoor-outdoor temperature difference, with CO<sub>2</sub> thermosyphons exhibiting higher heat transfer capacity than R22. When the filling ratio or indoor-outdoor temperature difference is small, a dry-out zone exists in the upper portion of the evaporator, which gradually disappears as the filling ratio or temperature difference increases. Energy-saving effect analysis results indicate that adopting CO<sub>2</sub> as the working fluid to replace R22 can significantly enhance the annual thermosyphon natural cooling time for data centers.

### Full Text

### Introduction

With the rapid development of the information industry, the number and energy consumption of data centers have grown dramatically. Currently, global data center energy consumption accounts for 1.1-1.5% of total worldwide energy consumption [1]. Among the components of data center energy consumption, cooling systems account for over 30% [2,3]. Therefore, reducing cooling energy

consumption has become an essential requirement for data center energy conservation, and relevant energy-saving cooling technologies have developed rapidly.

Traditional data center rooms rely on compressor work throughout the year to obtain cooling sources, consuming substantial electrical energy. For most regions in China, outdoor temperatures are below indoor temperatures for a considerable portion of the year. Utilizing natural low-temperature cold sources from the environment to cool data centers during these periods can save compressor energy consumption. This technology is called free cooling. Thermosyphon-based free cooling technology, as a heat transfer device, offers excellent phase-change heat transfer performance without compromising indoor air quality or humidity conditions, making it a promising free cooling method. In recent years, thermosyphon-based free cooling has attracted widespread attention, with many scholars conducting experimental and simulation studies on the performance of thermosyphons for free cooling under different structural configurations, operating conditions, and filling ratios [4-8]. Additionally, research has been conducted on the annual energy consumption characteristics of thermosyphon heat exchangers, as well as the influence of building envelope structures and set temperatures [9,10].

However, most current research uses Freon as the working fluid [4-10]. This type of working fluid is being phased out due to environmental considerations, making it imperative to investigate the performance under environmentally friendly working fluids for the future development and application of thermosyphon free cooling. CO<sub>2</sub>, as an environmentally friendly working fluid with favorable thermodynamic properties, is suitable as a replacement for Freon in this field. Currently, research on CO<sub>2</sub> thermosyphons remains very limited. Tong et al. [11,12] experimentally studied the performance of CO<sub>2</sub> thermosyphons, demonstrating that the heat transfer rate under CO<sub>2</sub> charge is higher compared to R22, with an optimal filling ratio of 100% based on evaporator internal volume. Given the limited research findings in this area and the fact that heat exchangers in these studies have been finned-tube types, it is necessary to investigate the performance of CO<sub>2</sub> thermosyphons, particularly under different heat exchanger configurations, and to explore their temperature and circulation flow characteristics.

This study focuses on a CO<sub>2</sub> thermosyphon with microchannel parallel-flow evaporators and condensers, investigating its performance and energy-saving effects under different filling ratios and operating conditions, and comparing it with R22 charging. To explore its circulation flow characteristics, infrared thermal imaging was employed to analyze the temperature distribution of the CO<sub>2</sub> thermosyphon. The research findings provide guidance for the design and application of CO<sub>2</sub> thermosyphons, particularly those employing microchannel parallel-flow heat exchangers.

## Experimental Setup

The experiments were conducted on a CO<sub>2</sub> separated thermosyphon with microchannel parallel-flow evaporators and condensers. An enthalpy difference laboratory was used for testing, with the experimental facility shown in [Figure 1: see original paper]. The evaporator was placed on the indoor side, while the condenser was placed on the outdoor side, maintaining a 1.0 m height difference to sustain working fluid circulation. A FLIR T610 thermal imaging camera was used to record the temperature distribution of the thermosyphon evaporator.

The structural parameters of the thermosyphon and experimental operating conditions are presented in . Both evaporators and condensers employed microchannel parallel-flow heat exchangers, while the riser and downcomer used copper pipes for air conditioning applications.

## Heat Transfer Analysis

The performance comparison between CO<sub>2</sub>-charged and R22-charged thermosyphons under different filling ratios is shown in [Figure 2: see original paper], with the indoor-outdoor temperature difference maintained at 10°C. As evident, the heat transfer rate of both CO<sub>2</sub> and R22 thermosyphons initially increases and then decreases with increasing filling ratio. The optimal filling ratio for CO<sub>2</sub> is approximately 150%, higher than that for R22. Under conditions below the optimal filling ratio, the heat transfer rate of the CO<sub>2</sub> thermosyphon decreases significantly, while above the optimal filling ratio, the heat transfer rate shows minimal variation. For R22, the optimal filling ratio is approximately 110%, with relatively small variations in heat transfer rate when deviating from this optimum, either higher or lower. This indicates that CO<sub>2</sub> thermosyphons are more suitable for larger working fluid filling ratios compared to R22 thermosyphons, with heat transfer rates being more significantly affected under low filling ratio conditions. Insufficient charging should be avoided.

The performance comparison between CO<sub>2</sub>-charged and R22-charged thermosyphons under different indoor-outdoor temperature differences is illustrated in [Figure 3: see original paper]. In the experiments, the filling ratios for CO<sub>2</sub> and R22 were 150% and 110%, respectively, representing their optimal values. As shown in [Figure 3: see original paper], the heat transfer rate of thermosyphons charged with both working fluids increases nearly linearly with increasing indoor-outdoor temperature difference. At the same temperature difference, the CO<sub>2</sub> thermosyphon demonstrates significantly higher heat transfer rates compared to R22. This confirms that CO<sub>2</sub> is suitable as an alternative working fluid for thermosyphon-based free cooling in data centers.

## Thermal Imaging Analysis

To further investigate the temperature distribution and circulation flow characteristics of the CO<sub>2</sub> thermosyphon, infrared thermal imaging analysis was conducted under different filling ratios and temperature differences. [Figure 4: see original paper] presents thermal images of the evaporator at different filling ratios with an indoor-outdoor temperature difference of 10°C. At lower filling ratios, the upper portion of the evaporator appears red (light-colored) in the thermal images, indicating higher wall temperatures than the lower section. This occurs because dryout occurs at a certain location as the working fluid flows upward through the evaporator, leaving the upper region filled with vapor-phase working fluid that cannot effectively cool the evaporator wall, resulting in elevated temperatures. As the filling ratio increases, the dryout region gradually diminishes and completely disappears at a filling ratio of approximately 150%. This explains why the optimal filling ratio is 150% as discussed above.

[Figure 5: see original paper] shows thermal images of the evaporator at different indoor-outdoor temperature differences with a filling ratio of 150%. When the temperature difference is small, a dryout region exists in the upper portion of the evaporator, but this region gradually disappears as the temperature difference increases. This is because at small temperature differences, the system has insufficient circulation driving force and low circulation flow rate, causing the working fluid to evaporate completely soon after being heated in the evaporator. The presence of the dryout region is thus one reason for the lower heat transfer rates observed at small temperature differences.

## Energy-Saving Analysis

The experimental results demonstrate that CO<sub>2</sub> as a working fluid for thermosyphon-based free cooling offers better heat transfer performance than the conventional R22 working fluid. To investigate the energy-saving prospects of CO<sub>2</sub> thermosyphons, this section analyzes their energy-saving effects in comparison with R22.

The relationship between cooling capacity and indoor-outdoor temperature difference for both CO<sub>2</sub> and R22 thermosyphons was fitted using the experimental results from [Figure 3: see original paper]:

$$Q_{CO_2} = -0.0020\Delta T^2 + 0.3695\Delta T - 0.8538 \quad (1)$$

$$Q_{R22} = 0.0017\Delta T^2 + 0.2717\Delta T - 1.1709 \quad (2)$$

where  $Q_{CO_2}$  and  $Q_{R22}$  are the cooling capacities of thermosyphons using CO<sub>2</sub> and R22 as working fluids, respectively, in kW; and  $\Delta T$  is the indoor-outdoor temperature difference in °C.

For a modular data center with an information equipment heat load of 4 kW and an indoor ambient temperature set at 27°C, the annual free cooling time using

thermosyphon-based free cooling equipment is defined as the total time when the thermosyphon cooling capacity exceeds the equipment heat load. Combining weather data for four cities—Harbin, Beijing, Shanghai, and Guangzhou [13], the calculated annual free cooling times for thermosyphons using CO<sub>2</sub> and R22 as working fluids are shown in [Figure 6: see original paper]. The results demonstrate that using CO<sub>2</sub> as the working fluid can significantly increase the annual thermosyphon free cooling time for data centers. Moreover, the improvement in free cooling time is more pronounced in southern China compared to northern regions.

## Conclusions

Thermosyphon-based free cooling technology represents an ideal method for energy-efficient cooling of data centers. This study investigated the system performance and energy-saving effects of a separated thermosyphon using CO<sub>2</sub> as the working fluid with microchannel parallel-flow evaporators and condensers, comparing it with R22. The main conclusions are as follows:

- (1) The optimal filling ratios for CO<sub>2</sub> and R22 are approximately 150% and 110%, respectively. Compared to R22, CO<sub>2</sub> is more suitable for larger working fluid filling ratios. The heat transfer rate of CO<sub>2</sub> thermosyphons decreases significantly under filling ratios below the optimum. The cooling capacity of thermosyphons charged with both working fluids increases with indoor-outdoor temperature difference, with CO<sub>2</sub> thermosyphons demonstrating greater heat transfer rates than R22 at the same temperature difference.
- (2) At lower filling ratios, a dryout region exists in the upper portion of the evaporator, which gradually diminishes as the filling ratio increases and completely disappears at a filling ratio of approximately 150%. When the indoor-outdoor temperature difference is small, a dryout region also exists in the upper evaporator section, but it gradually disappears as the temperature difference increases.
- (3) Substituting CO<sub>2</sub> for R22 can significantly increase the annual thermosyphon free cooling time for data centers. The improvement in free cooling time is more significant in southern China than in northern regions.

## References

- [1] Koomey J. Growth in Data Center Electricity Use 2005 to 2010 [R]. Oakland, CA: Analytics Press; 2011.
- [2] Ebrahimi K, Jones GF, Fleischer AS. Thermo-economic Analysis of Steady State Waste Heat Recovery in Data Centers Using Absorption Refrigeration[J]. Appl Energy 2015; 139: 62-64.

- [3] 安真. 数据中心的节能分析 [J]. 智能建筑电气技术, 2011, 5(5): 62-64. AN Zhen. Energy-saving Analysis Of Data Centers[J]. Electrical Technology of Intelligent Buildings, 2011, 5(5): 62-64.
- [4] 钱晓栋, 李震, 李志信. 数据机房热管空调系统的实验研究 [J]. 工程热物理学报, 2012, 33(7): 1217-1220. QIAN Xiaodong, LI Zhen, LI Zhixin. Experimental Study on Data Center Heat Pipe Air Conditioning System[J]. Journal of Engineering Thermophysics, 2012, 33(7): 1217-1220.
- [5] Zhang P, Wang B, Shi W, et al. Experimental Investigation on Two-Phase Thermosyphon Loop with Partially Liquid-Filled Downcomer[J]. Applied Energy, 2015, 160: 10-17.
- [6] Chehade A, Louahlia-Gualous H, Masson SL, et al. Experimental Investigations and Modeling of a Thermosyphon for Cooling with Zero Electrical Consumption[J]. Applied Thermal Engineering, 2015, 87: 2185-2190.
- [7] Zhang P, Wang B, Shi W, et al. Modeling and Performance Analysis of a Two-Phase Thermosyphon Loop with Partially/Fully Liquid-Filled Downcomer[J]. International Journal of Refrigeration, 2015, 58: 172-185.
- [8] Zhang H, Shao S, Xu H, et al. Simulation on the Performance and Free Cooling Potential of the Thermosyphon Mode in an Integrated System of Mechanical Refrigeration and Thermosyphon[J]. Applied Energy, 2017, 185: 1604-1612.
- [9] 周峰, 田昕, 马国远. IDC 机房用热管换热器节能特性实验研究 [J]. 土木建筑与环境工程, 2011, 33(1): 111-117. ZHOU Feng, TIAN Xin, MA Guoyuan. Energy-saving Performance of Thermosyphon Heat Exchanger Applied in Internet Data Center[J]. Journal of Civil, Architectural & Environmental Engineering, 2011, 33(1): 111-117.
- [10] Zhou F, Tian X, Ma G. Investigation into the Energy Consumption of a Data Center with a Thermosyphon Heat Exchanger[J]. Chinese Sci. Bull., 2011, 56 (20): 2185-2190.
- [11] Tong Z, Ding T, Li Z, et al. An Experimental Investigation of an R744 Two-Phase Thermosyphon Loop Used to Cool a Data Center[J]. Applied Thermal Engineering, 2015, 90: 201-208.
- [12] Tong Z, Liu X, Li Z, et al. Experimental Study on the Effect of Fill Ratio on an R744 Two-Phase Thermosyphon Loop[J]. Applied Thermal Engineering, 2016, 99: 302-312.
- [13] Song F, Zhu Q, Wu R, et al. Meteorological Data Set for Building Thermal Environment Analysis in China[C]//Proceedings of the 10th International Building Performance Simulation Association Conference and Exhibition. Beijing: 2007, 9-16.

*Note: Figure translations are in progress. See original paper for figures.*

*Source: ChinaXiv – Machine translation. Verify with original.*