

# Single-Layer Reflectarray Antennas with Improved Bandwidth by Attaching Phase-Delay Lines Postprint

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## Abstract

This paper proposes a novel X-band unit cell structure with improved bandwidth performance for single-layer microstrip reflectarray antennas. The proposed element comprises two circular rings, each incorporating a pair of gaps, with two phase-delay lines attached to the outer ring to provide the required phase shift. A 9 center-fed reflectarray antenna operating at 10 GHz is designed to validate the broadband performance of the proposed unit cell. Simulation results demonstrate a 1-dB gain bandwidth of 20% and a 3-dB gain bandwidth of 38.5%. The maximum gain at 10 GHz is 20.1 dB, corresponding to an aperture efficiency of 40%.

## Full Text

## Preamble

### Single-Layer Reflectarray Antennas with Improved Bandwidth by Attaching Phase-Delay Lines

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**Abstract—** A novel X-band unit cell structure with improved bandwidth performance for single-layer microstrip reflectarray antennas is proposed. The new element structure consists of two circular rings, each with a pair of gaps, and two phase-delay lines attached to the outer ring to provide the required phase shift. A 9×9 center-fed reflectarray antenna operating at 10 GHz is designed to validate the broadband performance of the proposed unit cell. Simulated

results show 20% 1-dB gain bandwidth and 38.5% 3-dB gain bandwidth. The maximum gain at 10 GHz is 20.1 dB, which is equivalent to 40% efficiency.

**Index Terms**— Broadband antenna, phase-delay line, reflectarray

## Introduction

Microstrip reflectarray technology has attracted wide attention in many applications, such as communication and radar, due to its alluring advantages [1]. However, there are some drawbacks associated with reflectarray antennas, among which narrow bandwidth is the most outstanding one. The narrow bandwidth performance of a microstrip reflectarray antenna is mainly due to two factors: first, the narrow bandwidth nature of the microstrip antenna element, and second, the differential spatial phase delays between the feed and elements in the reflectarray. For moderate-size reflectarrays, the first factor is more significant to the bandwidth limitation [2].

Many methods have been proposed to improve the bandwidth of the radiating element for reflectarray antennas in recent years. Using elements with a large-range linear phase response can increase the reflectarray bandwidth [3]. There are several ways to achieve linear phase response, such as using phase-delay lines [4], thick substrate, and multilayered structure [5]. Among these, the phase-delay line technique is appropriate, and numerous researches have been conducted regarding this technique [6], [8]. In this paper, a single-layer unit cell is developed to improve the bandwidth performance of reflectarray antennas. The unit cell is composed of two circular rings, each with a pair of gaps, and two phase-delay lines are attached to the outer ring to obtain a linear phase response. To reduce the cross polarization, a special arrangement for elements has been adopted, which was proposed in [6]. A  $9 \times 9$  center-fed reflectarray operating at X-band is designed to validate the broadband performance of the proposed unit cell. Simulated results show that 20% 1-dB gain bandwidth and 38.5% 3-dB gain bandwidth are achieved. The maximum gain at 10 GHz is 20.1 dB, which is equivalent to 40% efficiency.

## Unit Cell Design

The designed unit cell structure with single layer is shown in Fig. 1 [Figure 1: see original paper]. As can be seen, the proposed element is composed of two circular rings, each with a pair of gaps orthogonally placed, and two phase-delay lines are attached to the outer ring via stubs for phase shifts. The unit cell size is set to be  $L = 15$  mm, and the work frequency is designed to be 10 GHz.

To achieve better linear phase response, the distance between the inner ring and the outer ring is optimized. The stub width ( $w_s$ ) and the distance between the phase-delay line and the outer ring ( $L_s$ ) are optimized for good matching between phase-delay lines and the double-ring structure. After optimization, the final design element geometry parameters are listed in TABLE I.

The dimension of the unit cell is chosen to be  $0.5 \times 0.5$ . Elements are printed on a 1.5-mm-thick dielectric substrate with relative permittivity  $\epsilon_r = 4.4$  and backed by a 2-mm-thickness foam layer with relative permittivity  $\epsilon_r = 1$ .

To obtain the phase response of the element and optimize the parameters of the structure, an infinite array model is simulated using HFSS software with master-slave boundary and Floquet port excitation adopted.

The phase response curves versus the length of the phase-delay line are shown in Fig. 2(a) at different frequencies from 9 GHz to 12 GHz, in which the value of  $l$  represents the length of the phase-delay line of the element. As can be seen, a phase range of about  $550^\circ$  is achieved at the center frequency of 10 GHz. Parallel phase curves among different frequencies are also obtained. It is worth noting that when the value of  $l$  is between  $60^\circ$  and  $180^\circ$ , the phase curves have smaller slopes, which demonstrates better broadband performance compared with the radiating unit cells in [4], [5], [6].

To further investigate the broadband property of the designed unit cell, Fig. 2(b) [Figure 2: see original paper] shows the simulation results of the phase response versus frequency for different structures, i.e., the unit cell inner structure of the double rings with gaps and without gaps, which are resonant at the center working frequency. Obviously, the phase responses of the double-ring structures with gaps have smaller variation among the working frequency band of 8-14 GHz and show better linearity than that without gaps. The results indicate that by adding gaps, bandwidth performance of the reflectarray elements is improved [7].

## Reflectarray Design

In this section, in order to validate the broadband performance of the proposed unit cell, a  $9 \times 9$  center-fed reflectarray operating at X-band is designed and simulated.

The required phase shift for each unit cell is calculated at 10 GHz according to equation (1), where  $k$  is the propagation constant in free space,  $d_i$  is the distance from the phase center of the feed to the center of the  $i$ th unit cell in the reflectarray plane, and  $(\theta_0, \phi_0)$  is the designed main beam radiation direction of the reflectarray. The phase shifts are designed to compensate for the spatial delay between the feed and unit cells. Here, the phase shifts are calculated for  $(\theta_0, \phi_0) = (0^\circ, 0^\circ)$  at 10 GHz, which means that the designed main beam is normal to the reflectarray plane.

$$\phi_{R_i} = k_0 \cdot d_i - (x_i \cos \phi_0 + y_i \sin \phi_0) \sin \theta_0$$

The required phase distribution on the reflectarray aperture for the proposed reflectarray at 10 GHz is shown in Fig. 3 [Figure 3: see original paper]. The elements are arranged in a mirror symmetric configuration along the x-axis so

as to reduce the cross polarization [6], as shown in Fig. 4 [Figure 4: see original paper].

A pyramid horn is used as the feed of the reflectarray, which is positioned at 86 mm above the reflectarray plane. As Fig. 4 shows, the center-fed reflectarray is composed of 81 elements and has an aperture size of 135 mm  $\times$  135 mm. Simulations for the reflectarray antenna are carried out using CST Microwave Studio software and results are presented as follows.

The simulated co-polar and cross-polar (X-pol) radiation patterns of E-plane and H-plane at 10 GHz and 11 GHz are shown in Fig. 5 [Figure 5: see original paper] and Fig. 6 [Figure 6: see original paper], respectively. As can be seen, a maximum gain at 10 GHz of 20.1 dB is achieved, which is equivalent to 40% efficiency. Taking the E-plane pattern at 10 GHz for example, the simulated cross-polarization level is below  $-35$  dB, which is greatly reduced by the special element arrangement design. At the same time, the side lobe level is  $-13$  dB.

The simulated gain versus frequency is shown in Fig. 7 [Figure 7: see original paper], from which one can see that the 1-dB bandwidth is about 20% (9.74–11.7 GHz) and the 3-dB bandwidth is about 38.5% (9.45–13.3 GHz). The simulated results demonstrate that an obvious improvement in the bandwidth of the reflectarray antennas is achieved.

## Conclusion

A novel unit cell of single layer with improved bandwidth is proposed and designed for reflectarray antenna using phase-delay lines, and about  $550^\circ$  linear phase response is obtained. A  $9 \times 9$  center-fed reflectarray operating at X-band is then designed and simulated. The simulation results show that a maximum gain of 20.1 dB, which is equivalent to 40% efficiency at 10 GHz, is achieved. The results of 20% 1-dB bandwidth and 38.5% 3-dB bandwidth demonstrate improved bandwidth performance of the designed reflectarray compared with conventional reflectarrays with phase-delay lines.

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